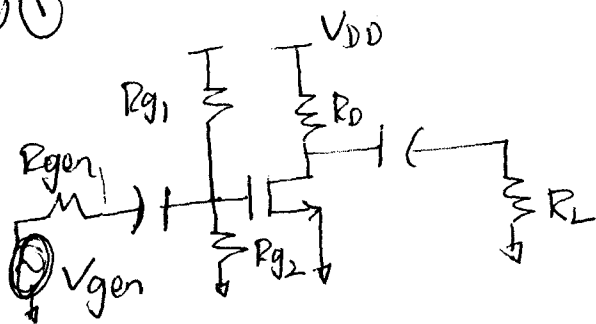


2) ①



$$\begin{aligned} V_{th} &= 0.3 \text{ Volts} \\ C_{ox} V_{sat} \mu_g &= 5 \text{ mS} \\ C_{gd} &= C_{gs} / 10 \\ R_{DS} &= \infty \\ f_c &= 200 \text{ MHz} \end{aligned}$$

$$\begin{aligned} R_{gen} &= 200 \text{ k}\Omega \\ R_{g1} \parallel R_{g2} &= 1 \text{ M}\Omega \\ I_{DQ1} &= 1 \text{ mA} \\ V_{DSQ1} &= 1 \text{ V} \\ A_{VMB} &= -10 \end{aligned}$$

$$I_{D1} = g_m (V_{gs} - V_{th}) = (5 \text{ mS})(V_{gs} - 0.3) \quad R_L = 2R_D$$

$$\Rightarrow V_{gs} = \frac{(1 \text{ mA})}{(5 \text{ mS})} + 0.3 = \underline{0.5 \text{ V}}$$

$$\text{Since } V_s = 0 ; \quad V_{th} = 0.5 \text{ V}$$

$$\text{Now, } \frac{V_{DD} \cdot R_{g2}}{R_{g1} + R_{g2}} = 0.5 \text{ V} \quad \& \quad R_{g1} \parallel R_{g2} = 1 \text{ M}\Omega \quad \begin{matrix} - (1) \\ - (2) \end{matrix}$$

Solving (1) & (2) simultaneously we get

$$R_{g1} = 8 \text{ M}\Omega \quad R_{g2} = 1.14 \text{ M}\Omega$$

where V_{DD} is found as follows:

$$A_{VMB} = -g_m (R_D \parallel R_L) = -10$$

$$\Rightarrow A_{VMB} = g_m (R_D \parallel 2R_D) = -10 \Rightarrow \frac{2}{3} g_m R_D = 10$$

$$\Rightarrow \underline{R_D = 3000 \Omega}$$

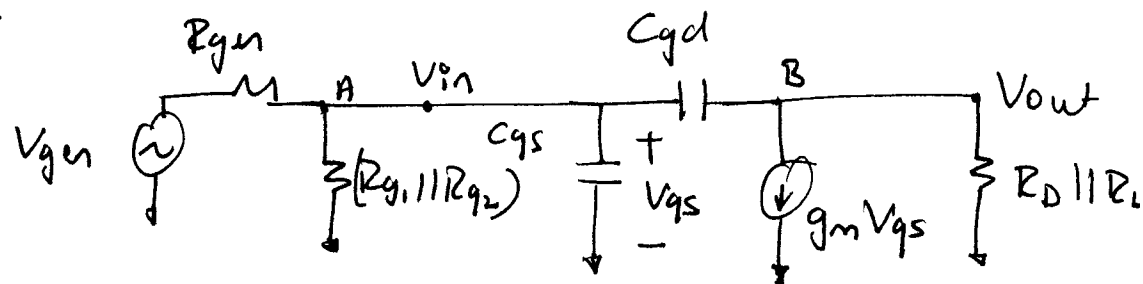
$$V_{DD} = V_{DSQ1} + I_D R_D = 1 \text{ V} + (1 \text{ mA})(3 \text{ k}\Omega) = \underline{4 \text{ V}}$$

$$f_c = \frac{1}{2\pi} \left(\frac{g_m}{C_{gs} + C_{gd}} \right) \Rightarrow C_{gs} + C_{gd} = \frac{g_m}{2\pi f_c} \quad \text{Also } C_{gd} = \frac{C_{gs}}{10}$$

$$1.1 C_{gs} = \frac{g_m}{2\pi f_c} \Rightarrow C_{gs} = \frac{g_m}{2\pi \times 1.1 \times f_c} = \underline{3.6 \text{ fF}}$$

$$\underline{C_{gd} = 0.36 \text{ fF}}$$

b).



KCL at node A gives:

$$\frac{(V_{in} - V_{gen})}{R_{gen}} + \frac{V_{in}}{(R_{g1} || R_{g2})} + \frac{(V_{in} - V_{out})}{(1/sC_{gd})} + \frac{V_{in}}{(1/sC_{gs})} = 0$$

$$V_{in} \left[\frac{1}{R_{gen}} + \frac{1}{R_{g1} || R_{g2}} + sC_{gd} + sC_{gs} \right] - V_{out} (sC_{gd})$$

$$= (V_{gen} / R_{gen}) \quad \text{--- (1)}$$

KCL at node B gives:

$$(V_{out} - V_{in}) sC_{gd} + g_m V_{gs} + \frac{V_{out}}{(R_D || R_L)} = 0$$

Noting that $V_{gs} = V_{in}$ we get

$$V_{in} [-sC_{gd} + g_m] + V_{out} [sC_{gd} + \frac{1}{R_D || R_L}] = 0 \quad \text{--- (2)}$$

$$\Rightarrow V_{in} = -V_{out} \left[\frac{sC_{gd} + \frac{1}{R_D || R_L}}{(g_m - sC_{gd})} \right] \quad \text{Substitute this into (1)}$$

$$(V_{out}) \left\{ \left[\frac{sC_{gd} + \frac{1}{R_D || R_L}}{g_m - sC_{gd}} \right] \left[\frac{1}{R_{gen}} + \frac{1}{R_{g1} || R_{g2}} + s(C_{gs} + C_{gd}) \right] - sC_{gd} \right\}$$

$$= \frac{V_{gen}}{R_{gen}}$$

$$\therefore \frac{V_{out}}{V_{gen}} = \left(\frac{1}{R_{gen}} \right) \left\{ \frac{1}{\left(sC_{gd} + \frac{1}{R_D || R_L} \right) \left[\frac{1}{R_{gen}} + \frac{1}{R_{g1} || R_{g2}} + s(C_{gs} + C_{gd}) \right] - sC_{gd}} \right\}$$

$$\therefore \frac{V_{out}}{V_{gen}} = \left(\frac{1}{R_{gen}} \right) \frac{(g_m - sC_{gd})}{\left(sC_{gd} + \frac{1}{R_D || R_L} \right) \left(\frac{1}{R_{gen}} + \frac{1}{R_{g1} || R_{g2}} + s(C_{gs} + C_{gd}) \right) - sC_{gd} \cdot (g_m - sC_{gd})}$$

$$\therefore \frac{V_{out}}{V_{gen}} = \frac{1}{R_{gen}} \cdot \left[\frac{(g_m - sC_{gd})}{\left(\frac{1}{R_D || R_L} \right) \left(\frac{1}{R_{gen}} + \frac{1}{R_{g1} || R_{g2}} \right) + s^2 (C_{gd} (C_{gs} + C_{gd})) + s \left[C_{gd} \cdot \left(\frac{1}{R_{gen}} + \frac{1}{R_{g1} || R_{g2}} \right) + (C_{gs} + C_{gd}) \left(\frac{1}{R_D || R_L} \right) \right]} \right]$$

Substituting $R_{g1} || R_{g2} = 1M\Omega$ $R_D || R_L = 2000$
 $C_{gs} = 3.6 \text{ pF}$ $C_{gd} = 0.36 \text{ pF}$ we get

$$\frac{V_{out}}{V_{gen}} = \frac{((5 \cdot 10^{-3}) - s(0.36 \cdot 10^{-15})) / (2000)}{(3 \cdot 10^{-9}) + (1.98 \cdot 10^{-18})s + (1.4256 \cdot 10^{-30})s^2}$$

This gives pole frequencies at

$$f_{P1} = 238 \text{ MHz} \quad f_{P2} = 219 \text{ GHz}$$

The zero frequency is at: $f_Z = \underline{2.2 \text{ THz}}$

→ The zero frequency is high enough to be neglected in analysis.

1.c) Since $f_{p1} = 238 \text{ MHz}$ is the dominant pole we rewrite the transfer function as:

$$\frac{V_{out}}{V_{in}} = \frac{-10}{1 + \tau_1 s} \quad \text{where } \tau_1 = \frac{1}{\omega_{p1}} = \underline{0.67 \text{ nsec}}$$

For $V_i(t) = 2 \text{ mV} \cdot u(t)$ $\xrightarrow{\mathcal{L}}$ $V_i(s) = \left(\frac{2 \text{ mV}}{s} \right)$ (Neglecting the 2nd pole)

$$V_{out}(s) = T(s) \cdot V_i(s)$$

$$= \frac{-10}{(1 + \tau_1 s)} \cdot \frac{(2 \text{ mV})}{s} = -\cancel{20 \text{ mV}} \cdot \left[\frac{k_1}{1 + \tau_1 s} + \frac{k_2}{s} \right]$$

As $s \rightarrow -1/\tau_1$ we get $k_1 = + (20 \text{ mV}) \tau_1$

As $s \rightarrow 0$ we get $k_2 = - (20 \text{ mV})$

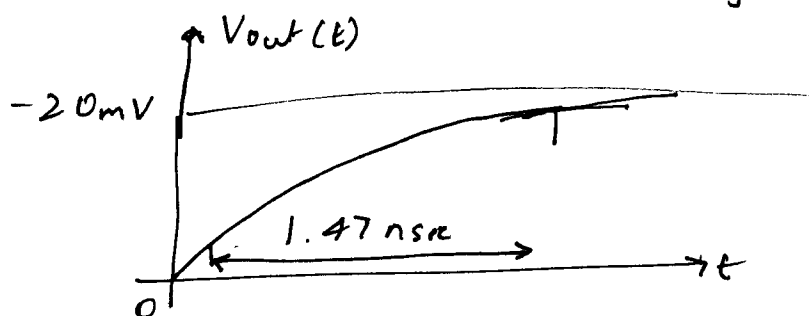
$$\therefore V_{out}(s) = \cancel{-20 \text{ mV}} \cdot \left[20 \text{ mV} \cdot \left[\frac{\tau_1}{1 + \tau_1 s} \right] - \frac{20 \text{ mV}}{s} \right]$$

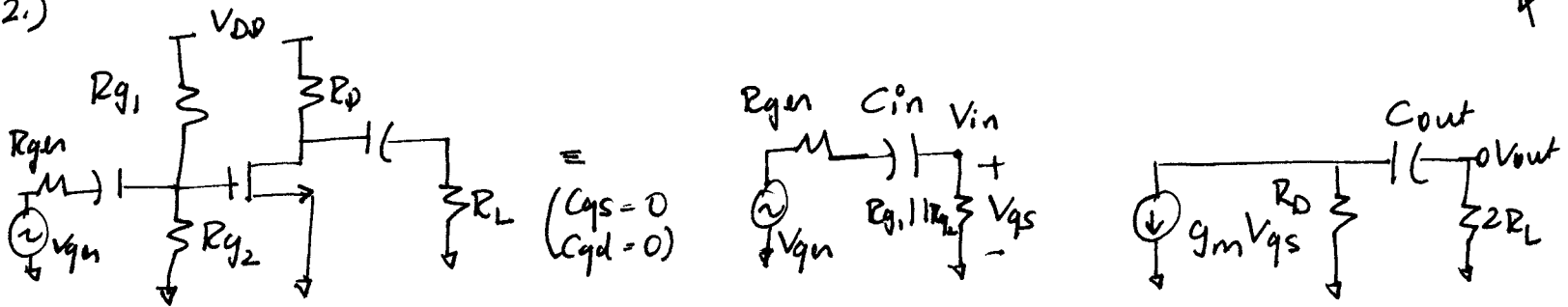
$$= -20 \text{ mV} \cdot \left[\frac{1}{s} - \frac{\tau_1}{1 + \tau_1 s} \right]$$

Taking inverse Laplace Transform we get

1d) $V_{out}(t) = - \left[20 \text{ mV} \cdot \left[1 - e^{-t/\tau_1} \right] u(t) \right]$ where $\tau_1 = 0.67 \text{ nsec}$

$$\tau_{10-90\%} = \tau \cdot \ln[0.9 \div 0.1] = \underline{1.47 \text{ nsec}}$$





$$V_{out} = g_m V_{gs} \cdot \left[R_D \parallel \left(2R_L + \frac{1}{sC_{out}} \right) \right]$$

$$= g_m V_{gs} \left[\frac{R_D \left(2R_L + \frac{1}{sC_{out}} \right)}{R_D + 2R_L + \frac{1}{sC_{out}}} \right]$$

And $V_{gs} = \frac{V_{gen} \cdot (R_{g1} \parallel R_{g2})}{(R_{g1} \parallel R_{g2}) + \frac{1}{sC_{in}} + R_{gen}}$

$$\therefore \left(\frac{V_{out}}{V_{gen}} \right) = g_m \cdot \left[\frac{(R_{g1} \parallel R_{g2})}{(R_{g1} \parallel R_{g2}) + R_{gen} + \frac{1}{sC_{in}}} \right] \left[\frac{R_D \cdot \left(2R_L + \frac{1}{sC_{out}} \right)}{R_D + 2R_L + \frac{1}{sC_{out}}} \right]$$

$$\therefore \frac{V_{out}}{V_{gen}} = g_m \cdot \left[\frac{sC_{in} \cdot (R_{g1} \parallel R_{g2})}{1 + sC_{in} (R_{gen} + (R_{g1} \parallel R_{g2}))} \right] \left[\frac{R_D \cdot (1 + s2R_L C_{out})}{1 + sC_{out} (R_D + 2R_L)} \right]$$

Substitute $R_{g1} \parallel R_{g2} = 1M\Omega$ $C_{in} = C_{out} = 5pF$

$R_{gen} = 200k\Omega$ $R_L = 6k\Omega$ $R_D = 3k\Omega$

we get

$$\frac{V_{out}}{V_{gen}} = (15) \left[\frac{s(5 \times 10^{-6})}{1 + s(6 \times 10^{-6})_{sec}} \right] \left[\frac{(3 \times 10^3)(1 + s(6 \times 10^{-8})_{sec})}{1 + s(7.5 \times 10^{-8})_{sec}} \right]$$

$$= \frac{(15s)_{sec} [5 \times 10^{-6} + s(3 \times 10^{-13})_{sec}]}{[1 + s(6 \times 10^{-6})_{sec}] [1 + s(7.5 \times 10^{-8})_{sec}]}$$

This gives the pole frequencies at

$$f_{P1} = 26 \text{ kHz}$$

$$f_{P2} = 2 \text{ MHz}$$

2.) The transfer function can be written as:

$$\frac{V_{out}}{V_{in}} = \frac{V_o}{V_{in}} \Big|_{MB} \left[\frac{s \tau_{in}}{1 + s \tau_{in}} \right] \left[\frac{s \tau_{out}}{1 + s \tau_{out}} \right]$$

where

$$\tau_{in} = C_{in} (R_{gen} + R_{g1} \parallel R_{g2}) = 6 \text{ } \mu\text{sec}$$

$$\tau_{out} = C_{out} (R_D + 2R_D) = 45 \text{ nsec}$$

$$\frac{V_o}{V_{in}} \Big|_{MB} = -10$$

Step response of amplifier:

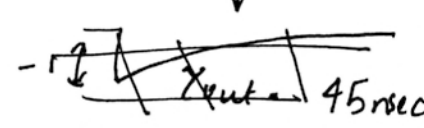
$$V_{in}(s) = \frac{1 \text{ mV}}{s} \rightarrow V_{in}(t) = (1 \text{ mV}) u(t)$$

Then

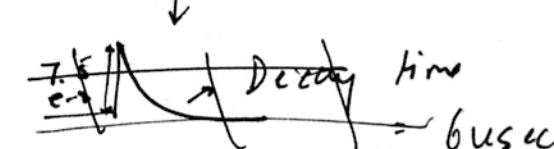
$$V_{out}(s) = \left(\frac{\tau_{in}}{1 + s \tau_{in}} \right) \cdot \left(\frac{\tau_{out}}{1 + s \tau_{out}} \right) \cdot (s) \cdot (A_{VMB}) \cdot (1 \text{ mV})$$

$$= (A_{VMB})(1 \text{ mV}) \left[\underbrace{\frac{\tau_{in}}{\tau_{in} - \tau_{out}}}_{1.00} \cdot \frac{\tau_{out}}{1 + s \tau_{out}} + \underbrace{\frac{\tau_{out}}{\tau_{out} - \tau_{in}}}_{(-7.5 \times 10^{-3})} \cdot \frac{\tau_{in}}{1 + s \tau_{in}} \right]$$

$$\therefore V_{out}(t) = -(10 \text{ mV}) \left[(1.00) e^{-t/\tau_{out}} - (7.5 \times 10^{-3}) e^{-t/\tau_{in}} \right]$$

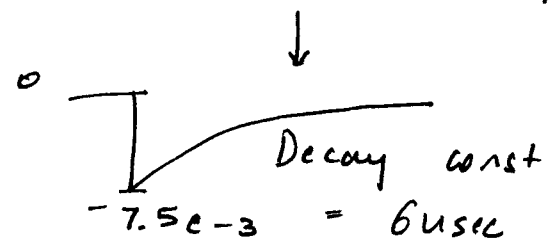
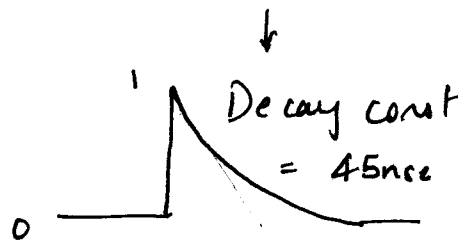


$\tau_{out} = 45 \text{ nsec}$



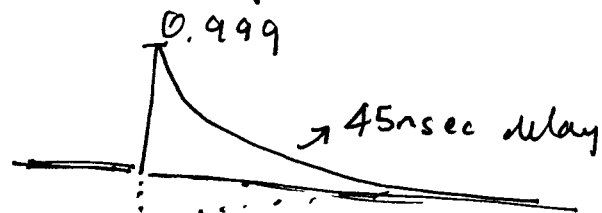
Decay time = $6 \text{ } \mu\text{sec}$

$$V_{OUT}(t) = -10\text{mV} \cdot \left[1.00 e^{-t/\tau_{out}} - (7.5e-3) e^{-t/\tau_{in}} \right]$$

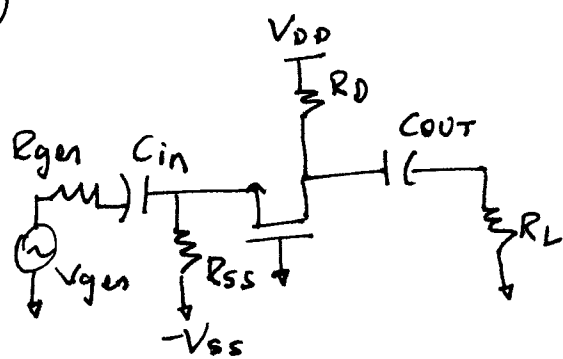


(Curves normalized to gain)

Total step response



The lower of the two frequency poles contributes only a small amount to the step response. → Step response is dominated by the high frequency pole.



$$\begin{aligned}
 V_{DD} &= 1.5V & -V_{SS} &= -1.5V \\
 V_{sat} C_{ox} W_g &= 10 \text{ mA/V} & V_{th} &= 0.5V \\
 V_D &= 0.5V & I_D &= 1 \text{ mA} \\
 R_L &= 3 R_D & R_{gen} &= 50 \Omega \\
 C_{gs} &= 10 * C_{gd} & f_T &= 150 \text{ MHz} \\
 W_{ds} &= \frac{g_m}{50}
 \end{aligned}$$

Design:

$$V_D = V_{DD} - I_D R_D \Rightarrow R_D = \frac{V_{DD} - V_D}{I_D}$$

$$\therefore R_D = \left(\frac{1.5V - 0.5V}{1 \text{ mA}} \right) = \boxed{1 \text{ k}\Omega}$$

$$\Rightarrow \boxed{R_L = 3 R_D = 3 \text{ k}\Omega}$$

Also, $I_D = g_m [V_{gs} - V_{th}] \Rightarrow V_{gs} = \frac{I_D}{g_m} + V_{th}$

Since $V_g = 0 \Rightarrow V_s = - \left[\frac{I_D}{g_m} + V_{th} \right] = - \left[\frac{1 \text{ mA}}{10 \text{ mA/V}} + 0.5V \right]$

$$\Rightarrow V_s = - 0.6 \text{ Volts.}$$

Now, $V_s = -V_{SS} + I_D R_s \Rightarrow R_s = \frac{V_s + V_{SS}}{I_D}$

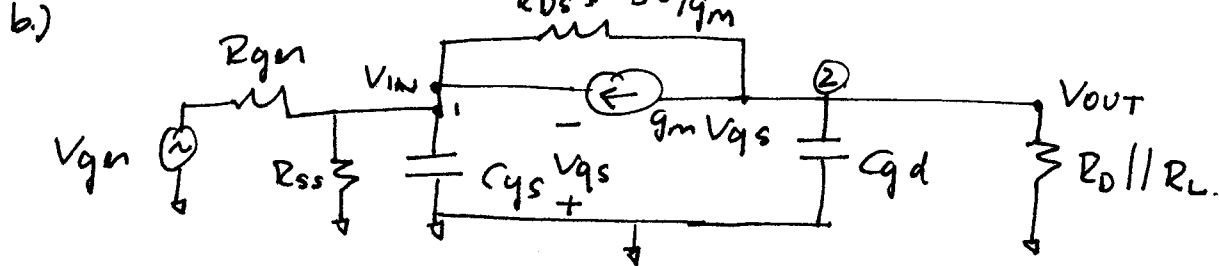
$$\Rightarrow \boxed{R_s = 900 \Omega}$$

$$= \frac{+(0.6 + 1.5)V}{1 \text{ mA}}$$

$$f_T = \frac{g_m}{2\pi [C_{gs} + C_{gd}]} \Rightarrow 11 C_{gd} = \frac{g_m}{\omega_T}$$

$$\Rightarrow C_{gd} = 0.964 \text{ fF}$$

$$C_{gs} = 9.64 \text{ fF}$$



KCL at node 1:

$$\left(\frac{V_{in} - V_{gs}}{R_{gm}} \right) + \frac{V_{in}}{R_{ss}} + V_{in}(sC_{gs}) - g_m V_{gs} + (V_{in} - V_{out})C_{ds} = 0$$

$$\therefore V_{in} \left[\frac{1}{R_{gm}} + \frac{1}{R_{ss}} + sC_{gs} + g_m + C_{ds} \right] + V_{out} [-C_{ds}] = \frac{V_{gs}}{R_{gm}} \quad \text{--- (1)}$$

KCL at node 2:

$$g_m V_{gs} + (V_{out} - V_{in})C_{ds} + V_{out}(sC_{gd}) + \frac{V_{out}}{(R_D || R_L)} = 0$$

$$\therefore V_{out} [C_{ds} + sC_{gd} + C_{L}] + V_{in} [-C_{ds} - g_m] = 0 \quad \left(C_L = \frac{1}{R_D || R_L} \right)$$

$$\therefore V_{in} = V_{out} \left[\frac{C_{ds} + C_L + sC_{gd}}{g_m + C_{ds}} \right] \quad \text{--- (2)}$$

Put (2) into (1) to get

$$V_{out} \left\{ \left[\frac{C_{ds} + C_L + sC_{gd}}{g_m + C_{ds}} \right] \left[\frac{1}{R_{gm}} + \frac{1}{R_{ss}} + sC_{gs} + g_m + C_{ds} \right] - C_{ds} \right\}$$

$$\therefore \frac{V_{out}}{V_{gs}} = \left(\frac{g_m + C_{ds}}{R_{gm}} \right) \left[\frac{1}{(C_{ds} + C_L + sC_{gd}) \left(\frac{1}{R_{gm}} + \frac{1}{R_{ss}} + sC_{gs} + g_m + C_{ds} \right)} - (g_m + C_{ds})C_{ds} \right]$$

$$\therefore \frac{V_{out}}{V_{gs}} = (2.04 \times 10^{-4}) \left[\frac{1}{[1.5e-3 + s(0.964 \text{ fF})] [0.0313 + s(1.64 \text{ fF}) - (2.04e-6)]} \right]$$

b.) NOTE: With R_D s very high the circuit can be solved as has been shown in the notes

However, with R_D s significantly smaller, we will have to use nodal analysis to reach the solution

$$\frac{V_{OUT}}{V_{IN}} = \frac{(2.04 \times 10^{-4})}{(4.7 \times 10^{-5}) + s(0.0446 \times 10^{-15}) + s^2(9.3 \times 10^{-30}) - (2.04 \times 10^{-6})}$$

$$= \frac{2.04 \times 10^{-4}}{(4.49 \times 10^{-5}) + s(0.044 \times 10^{-15}) + s^2(9.3 \times 10^{-30})}$$

$$= \frac{4.54}{1 + (9.8 \times 10^{-13})s + (2 \times 10^{-25})s^2}$$

∴ Poles will correspond to s values of

$$s_1 = -1.44 \times 10^{12} \quad s_2 = -3.45 \times 10^{12}$$

Put $s = j\omega$ to get

$$\omega_{P1} = 1.44 \times 10^{12} \text{ R/sec}$$

which corresponds to :

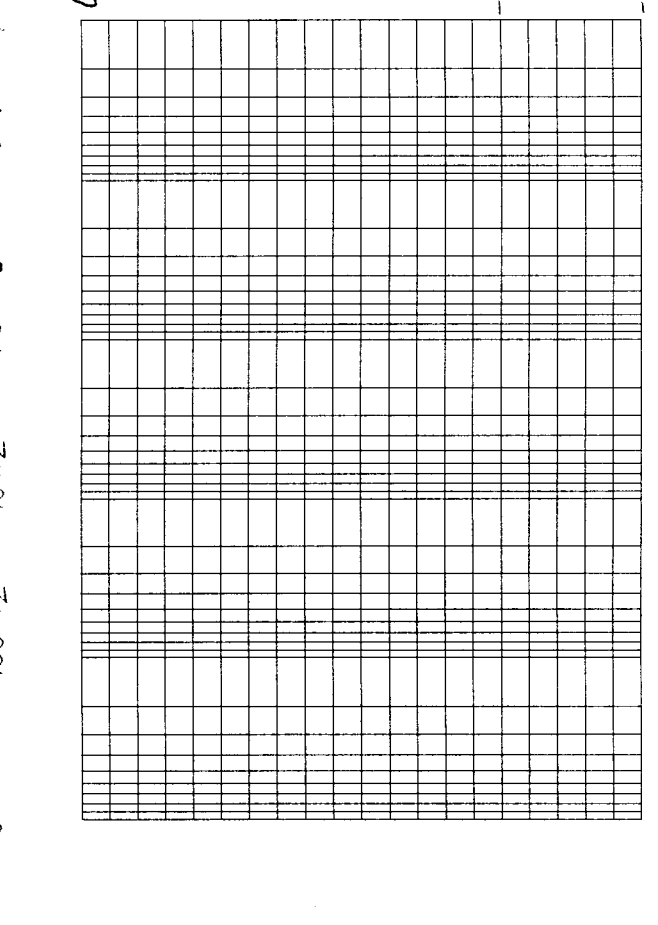
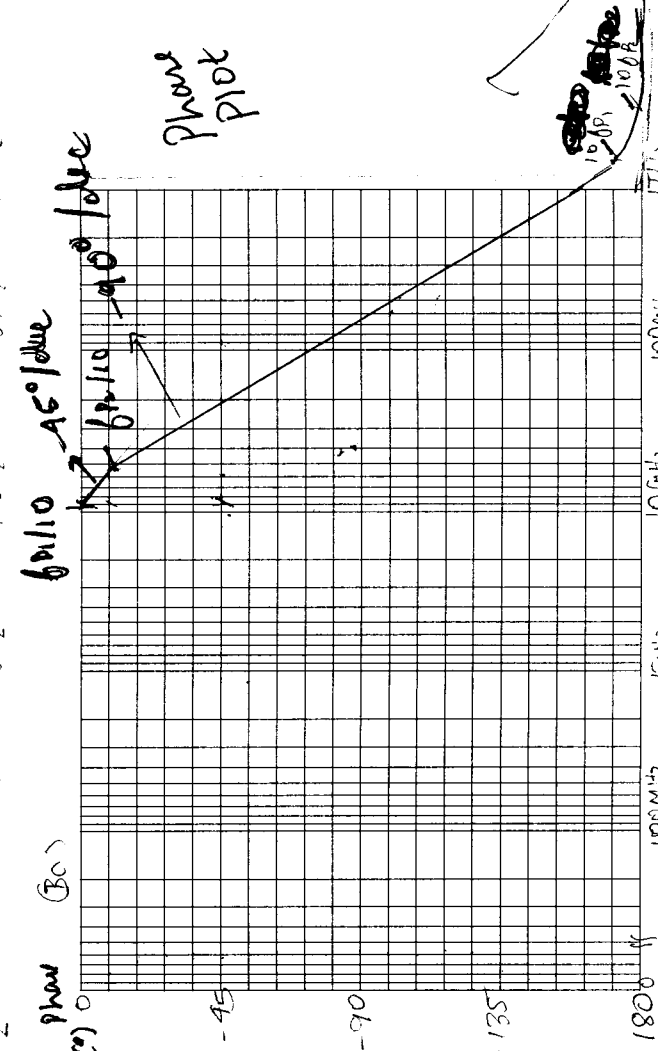
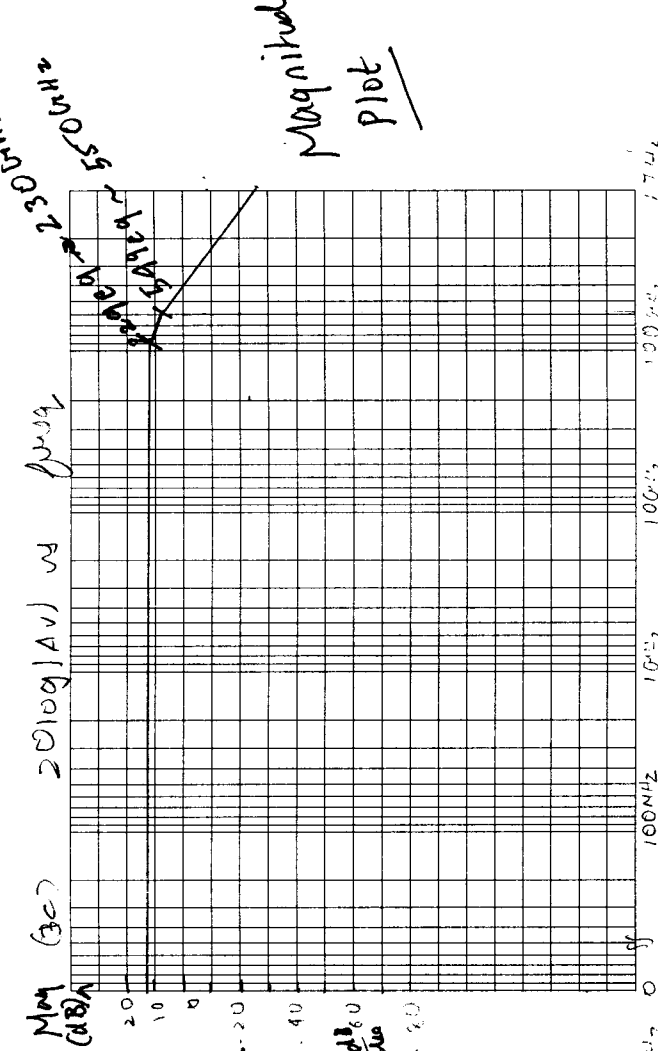
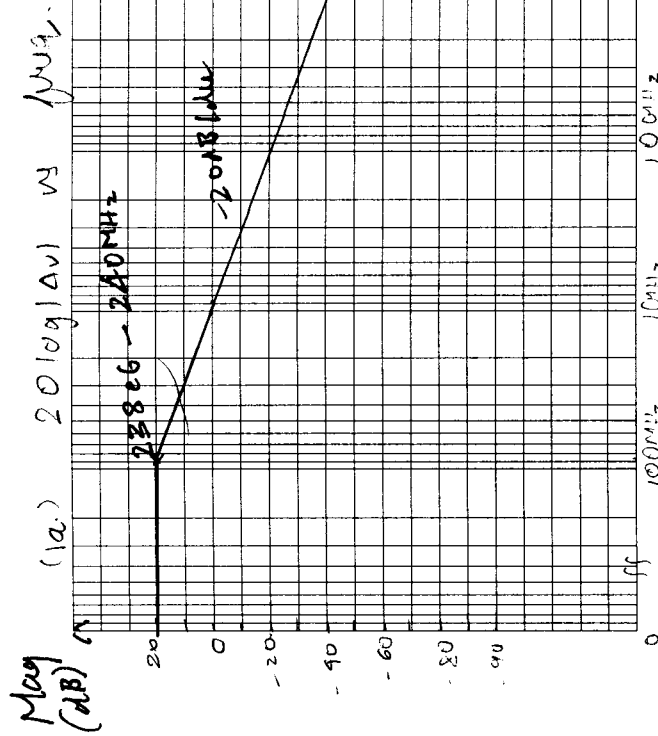
$$f_{P1} = \frac{0.229 \times 10^{12} \text{ Hz}}{}$$

$$f_{P1} = 229 \text{ MHz}$$

$$\omega_{P2} = 3.45 \times 10^{12} \text{ R/sec}$$

$$f_{P2} = \frac{0.549 \times 10^{12} \text{ Hz}}{}$$

$$f_{P2} = 549 \text{ MHz}$$



Magnitud
Plot

Phase
Plot