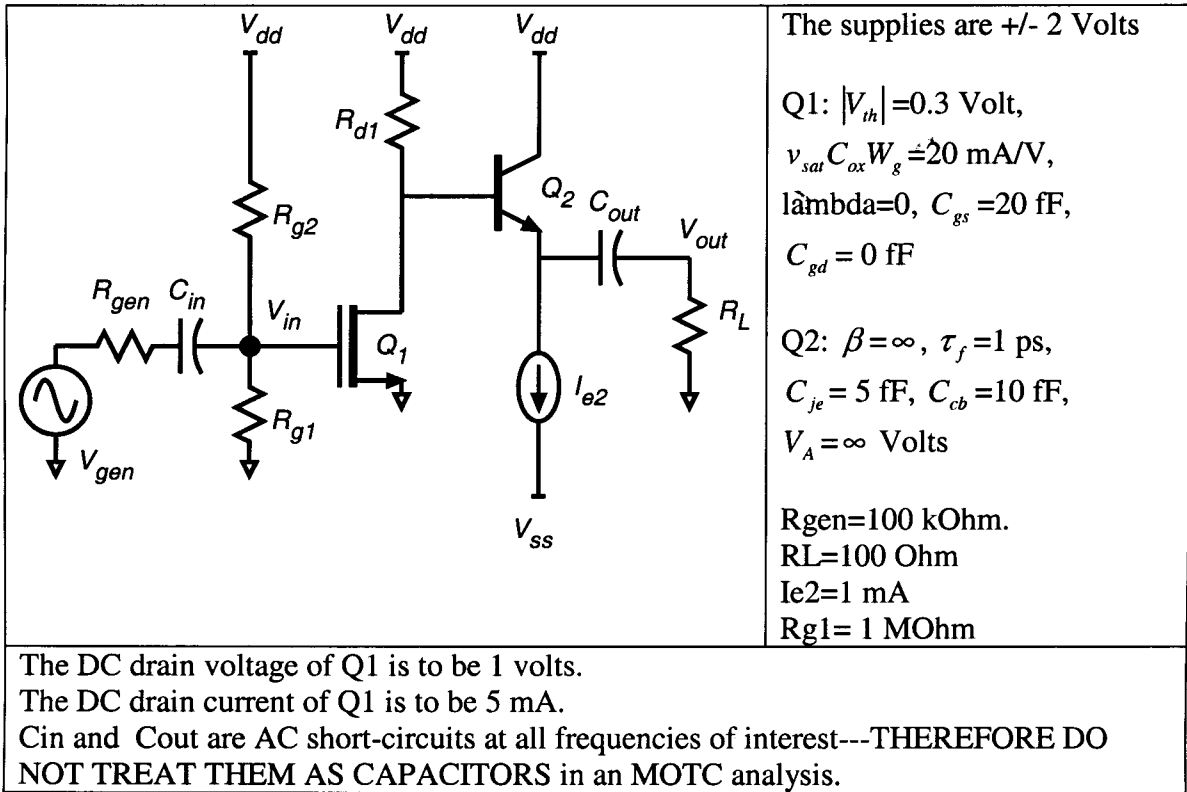


MID TERM A SOLUTIONS

Problem 1, 70 points



$$R_{d1} = \frac{(V_{dd} - V_d)}{I_D} \quad \frac{V}{A}$$

$$I_D = 5 \text{ mA}$$

$$V_d = \text{dc drain voltage} = 1 \text{ V}$$

$$R_{d1} = \frac{(2 - 1) \text{ V}}{5 \text{ mA}} = \frac{1 \text{ V}}{5 \text{ mA}} = 200 \text{ }\Omega$$

$$I_D = g_m \left(\frac{A}{V} \right) (V_{gs} - V_{th}) \text{ V} \Rightarrow \frac{I_D}{g_m} \frac{A}{V} = (V_{gs} - V_{th}) \text{ V}$$

$$\frac{5 \text{ mA}}{20 \text{ mA/V}} = V_{gs} - 0.3 \Rightarrow \left(\frac{1}{4} + 0.3 \right) \text{ V} = V_{gs}$$

$$V_{gs} = 0.55 \text{ V}$$

2 See next page

Part a, 10 points

Find the following

$$R_{g2} = \underline{4.45 \text{ M}\Omega} \quad R_{d1} = \underline{200 \Omega}$$
$$(C_{je} + C_{diff}) \text{ of } Q2 = \underline{43.5 \text{ fF}}$$

$$I_{Rg1} = \frac{V_g (\text{V})}{R_{g1} (\text{A})}$$

$$V_g = V_{gs} = 0.55 \text{ V}$$

$$I_{Rg1} = \frac{0.55 \text{ V}}{1 \text{ M}\Omega} = 0.55 \mu\text{A}$$

$$R_{g2} = \frac{V_{dd} - V_g (\text{V})}{I_{Rg1} (\text{A})} = \frac{(2 - 0.55) \text{ V}}{0.55 \mu\text{A}}$$

$$R_{g2} = \frac{1.45 \text{ V}}{0.55 \mu\text{A}} = 2.64 \text{ M}\Omega$$

$$C_{be} = g_m T_f + C_{je}$$

$$C_{be} = \frac{1 \text{ mA}}{26 \text{ mV}} \times 1 \text{ pS} + 5 \text{ fF}$$

$$C_{be} = 43.5 \text{ fF}$$

$$1 \text{ fF} = 10^{-15} \text{ F}$$

3

Part b, 10 points

Mid Band Analysis:

Find the mid-band small signal voltage gain of Q2 (the small signal voltage at the emitter of Q2 divided by the small signal voltage at the base of Q2)

$$A_{v2} = \underline{0.7936}$$

Find the mid-band small signal voltage gain of Q1 (the small signal voltage at the drain of Q1 divided by the small signal voltage at the gate of Q1)

$$A_{v1} = \underline{-4}$$

Find V_{in}/V_{gen}

$$V_{in}/V_{gen} = \underline{0.8909}$$

$$\textcircled{2} \left[\frac{V_{in}}{V_{gen}} = \frac{2.64 \text{ M}\Omega \parallel 1 \text{ M}\Omega}{100 \text{ k}\Omega + 2.64 \text{ M}\Omega \parallel 1 \text{ M}\Omega} = \frac{0.72527 \text{ M}}{100 \text{ k}\Omega + 0.72527 \text{ M}} \right]$$

$$\frac{V_{in}}{V_{gen}} = 0.87836 \quad \textcircled{1}$$

$$A_{v1} = -g_m R_{eq} = \frac{-20 \text{ mA}}{V} \times (R_{d1}) \Omega \quad \textcircled{1}$$
$$A_{v1} = -0.02 \times 200 \Omega = -4 \quad \textcircled{4}$$

$$\textcircled{4} \left[A_{v2} = \frac{R_{Leq}}{R_{Leq} + r_{e2}} = \frac{100 \Omega}{100 \Omega + \frac{26 \text{ mV}}{1 \text{ mA}}} = \frac{100}{126} \right]$$
$$A_{v2} = 0.7936$$

Part c: 20 points

USING MOTC, you will find the two dominant pole frequencies of the transfer function.

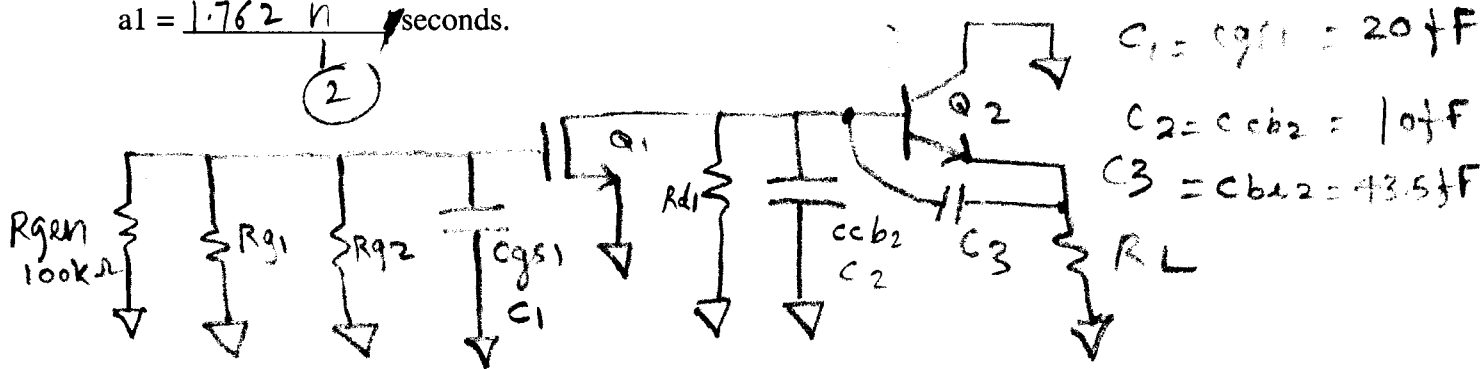
Give the frequencies of these in Hz:

Component of a_1 due to C_{gs} of transistor Q1 = 1.757 n seconds.

Component of a_1 due to C_{cb} of transistor Q2 = 2 p seconds.

Component of a_1 due to $(C_{je} + C_{diff})$ of transistor Q2 = 2.693 seconds.

$a_1 = \underline{1.762 \text{ n}}$ seconds.



$$R_{11}^{\circ} = R_{gen} \parallel R_{g1} \parallel R_{g2} = 100k\Omega \parallel 1M\Omega \parallel 2.64M\Omega$$

$$R_{11}^{\circ} = 87.88 k\Omega$$

$$R_{22}^{\circ} = R_{d1} = 200\Omega$$

$$R_{33}^{\circ} = R_{d1} (1 - A_2) + R_2 \parallel R_L$$

$$= 200\Omega (1 - 0.7936) + 26\Omega \parallel 100\Omega$$

$$= 41.28\Omega + 20.63\Omega$$

$$R_{33}^{\circ} = 61.9\Omega$$

$$[R_{11}^{\circ} C_1 = R_{11}^{\circ} C_{gs1} = (87.88 k\Omega) 20 fF = 1757.6 psec \quad (1)]$$

$$[R_{22}^{\circ} C_2 = (200\Omega) 10 fF = 2 psec \quad (1)]$$

$$[R_{33}^{\circ} C_3 = (61.915\Omega) 43.5 fF = 2.693 psec \quad (1)]$$

$$a_1 = R_{11}^{\circ} \Omega C_1 F + R_{22}^{\circ} \Omega C_2 F + R_{33}^{\circ} \Omega C_3 F = 1762.293 psec$$

Component of a_2 due to C_{gs1} and $C_{cb2} = \underline{3.515 \times 10^{-21} \text{ seconds}^2}$.

Component of a_2 due to C_{gs1} and $(C_{je} + C_{diff}) = \underline{4.733 \times 10^{-21} \text{ seconds}^2}$.

Component of a_2 due to C_{cb2} and $(C_{je} + C_{diff}) = \underline{1.795 \times 10^{-24} \text{ seconds}^2}$.

$$a_2 = \underline{8.25 \times 10^{-21} \text{ seconds}^2}$$

$$f_{p1} = \underline{33.87 \text{ GHz}}, f_{p2} = \underline{90.5 \text{ MHz}}$$

①

①

$$a_2 = (R_{11}^0 C_1 C_2 R_2' + R_{11}^0 C_1 C_3 R_33' + R_{22}^0 C_2 C_3 R_33') \text{ sec}^2 \quad \rightarrow \text{①}$$

$$\text{②} [R_{22}' = R_{22}^0 = 200 \Omega ; R_{33}^2 = (R_L \parallel R_L) \Omega = (26 \Omega) \parallel 100 \Omega$$

$$= 20.635 \Omega$$

$$\text{③} [R_{33}' = R_{33}^0 = 61.9 \Omega$$

$$\text{④} [R_{11}^0 C_1 C_2 R_{22}' = (87.88 \text{ k}\Omega)(200 \Omega)(20 \text{ fF})(10 \text{ fF})$$

$$= (7.030 \times 10^9 \times 10^{-15} \times 10^{-15}) \text{ sec}^2$$

$$[R_{11}^0 C_1 C_2 R_{22}' = 3.515 \times 10^{-21} \text{ sec}^2$$

$$R_{11}^0 C_1 C_3 R_{33}' = (87.88 \text{ k}\Omega)(61.9 \Omega)(20 \text{ fF} \times 43.5 \text{ fF}) \quad \text{②}$$

$$R_{11}^0 C_2 C_3 R_{33}^2 = 4.733 \times 10^{-21} \text{ sec}^2 \quad \text{①}$$

$$R_{22}^0 C_2 C_3 R_{33}^2 = 200 \Omega (20.635 \Omega)(10 \text{ fF})(43.5 \text{ fF})$$

$$R_{22}^0 C_2 C_3 R_{33}^2 = 1.795 \times 10^{-24} \text{ sec}^2 \quad \text{①}$$

$$a_2 = 8.249 \times 10^{-21} \text{ sec}^2 - \text{from ①}$$

$$[a_2 = (3.515 \times 10^{-21} + 4.733 \times 10^{-21} + 1.795 \times 10^{-24}) \text{ sec}^2] \text{ See next pag. for } f_{p1} \text{ and } f_{p2}$$

$$1 + a_1 s + a_2 s^2 = 0$$

$$a_1 = 1762.3 \text{ psec}$$

$$a_2 = 8.249 \times 10^{-21} \text{ sec}^2$$

$$s_2 = -2.130 \times 10^{11}$$

$$s_1 = -1.741 \times 10^{-9} = -5.6915 \times 10^8$$

$$fp_2 = \frac{18.11}{2\pi} - \left(\frac{2.13 \times 10^{11}}{2\pi} \right) Hz = 33.867 \text{ GHz}$$

$$\begin{aligned} fp_1 &= \frac{18.21}{2\pi} - \left(5.6915 \times 10^8 \times 0.159 \right) Hz \\ &= 90.5 \times 10^6 Hz \\ &= 90.5 MHz \end{aligned}$$

Part e: 10 points

The circuit has 2 zeros its transfer function.

Give the frequencies of these in Hz:

$$f_{z1} = \underline{\quad\quad\quad}$$

$$f_{z2} = \underline{140.58 \text{ GHz}}$$

$$b_1 = -\frac{C_{gd}}{g_m} = \frac{0}{g_m} = 0 \text{ sec}$$

$$f_{z1} = \frac{1}{2\pi b_1} = \infty$$

$$\textcircled{5} \quad b_2 = \frac{C_{be}}{g_m} = \frac{43.5 \text{ fF}}{\frac{1}{26}} = 1131 \times 10^{-15} \text{ sec} = 1.131 \text{ psec}$$

$$\textcircled{4} \quad f_{z2} = \frac{1}{2\pi b_2} = \frac{1}{2\pi \times 1.131 \text{ psec}}$$

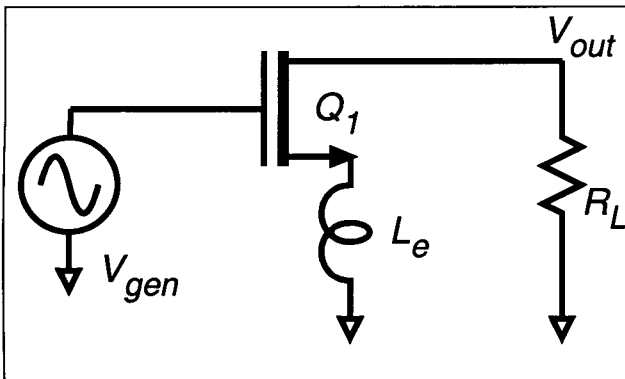
$$= 0.159 \times \left(\frac{10^{12}}{1.131} \right)$$

$$f_{z2} = 140.58 \times 10^{11} \text{ Hz}$$

$$\textcircled{1} \quad f_{z2} = 140.58 \text{ GHz}$$

Problem 2, 30 points

Part a 10 points



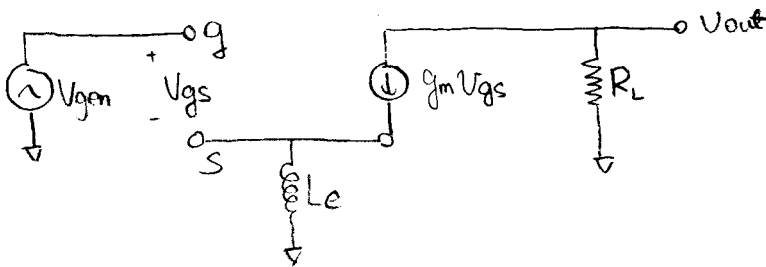
Small signal analysis.

Ignore the DC bias; you don't need it.

The FET has $\lambda=0$ hence $G_{ds}=0$. Also, $C_{gs}=C_{gd}=0$ fF

Replacing the transistor with its high frequency small-signal model, draw a small-signal equivalent circuit diagram.

iii Small-Signal Model



hard to give partial credit.

Grading Rules as following

1. No labels for current source -5
2. wrong sign of voltage expression in current source
3. wrong voltage labels in schematic -5

Part b, 10 points

USING NODAL ANALYSIS, compute $V_{out}(s)/V_{gen}(s)$ in ratio-of-polynomials form:

$$\frac{V_{out}(s)}{V_{gen}(s)} = \left. \frac{V_{out}}{V_{gen}} \right|_{\text{mid-band}} \times \frac{1 + b_1 s + b_2 s^2 + \dots}{1 + a_1 s + a_2 s^2 + \dots} = \frac{-g_m R_L \cdot \frac{1}{1 + g_m L_e s}}{1}$$

② at S node

$$\textcircled{3} \left[\frac{V_s}{s L_e} = g_m V_{gs} \quad , \text{ where } V_{gs} = V_g - V_s = V_{gen} - V_s \right]$$

$$\Rightarrow V_s = \frac{s g_m L_e}{1 + s g_m L_e} V_{gen} \quad \text{--- ①}$$

③ at output node

$$\textcircled{3} \left[\frac{V_{out}}{R_L} + g_m V_{gs} = 0 \right]$$

$$\Rightarrow V_{out} = -g_m R_L (V_{gen} - V_s) \quad \text{--- ②}$$

④ From ① and ②

$$V_{out} = -g_m R_L \left(V_{gen} - \frac{s g_m L_e}{1 + s g_m L_e} V_{gen} \right)$$

$$\begin{aligned} \Rightarrow \frac{V_{out}(s)}{V_{gen}(s)} &= \left. \frac{V_{out}}{V_{gen}} \right|_{\text{mid-band}} \times \frac{1 + b_1 s + b_2 s^2 + \dots}{1 + a_1 s + a_2 s^2 + \dots} \\ &= -g_m R_L \times \frac{1}{1 + g_m L_e \cdot s} \quad \text{--- ④} \end{aligned}$$

Part c, 10 points

$g_m = 100 \text{ mS}$. $R_L = 1 \text{ k}\Omega$. $L_e = 1 \text{ nH}$

Find the frequencies of any zeros (there may be zero, one or two present) in the transfer function:

$f_{z1} = \underline{\hspace{2cm}}$, $f_{z2} = \underline{\hspace{2cm}}$,

There may be either 1 or 2 poles of the transfer function.

If the poles are real, give the 1 or 2 pole frequencies in Hz:

$f_{p1} = \underline{1.59 \text{ GHz}}$, $f_{p2} = \underline{\hspace{2cm}}$

If there are 2 poles, and they are complex, give $f_n = \omega_n / 2\pi$ and the damping factor ζ :

$f_n = \omega_n / 2\pi = \underline{\hspace{2cm}}$, $\zeta = \underline{\hspace{2cm}}$

⑩ From part b

$$\frac{V_{out}(s)}{V_{gen}(s)} = -g_m R_L \times \frac{1}{1 + j \frac{f}{f_p}} \quad \text{where } f_p = \frac{0.159}{g_m \cdot L_e}$$
$$= \frac{0.159}{100(\text{mS}) \cdot 1(\text{nH})}$$
$$= 1.59 \times 10^9 (\text{Hz})$$
$$= 1.59 (\text{GHz})$$

$$g_m R_L = 100(\text{mS}) \cdot 1(\text{k}\Omega)$$
$$= 100$$

⑪ [There is a real pole at $f_p = 1.59 (\text{GHz})$.

deduct points 2 each for additional poles and zeros