

Today: State (Space) Feedback

Lecture 11

ECE 147B

Digital Control

Reading: FPW 7.2, 8.1
or: FV 6.5, (9.1), 9.2

Topics:

- Quick, last-minute REVIEW! ("Pop Quiz")
- "Direct Design" revisited: unstable poles in $G(z)$?
- State space block diagrams
- Modeling the ZOH via ss equations
- State feedback: $u = -Kx$
- Control Canonical Form

Next Class: MIDTERM EXAM.



- You may bring one, single-single, self-prepared 8 ½ x 11 sheet of notes. No calculators, cell phones, etc.

Pop Quiz!

Say $X_A = \frac{z}{z+1}$ $X_B = (\frac{z}{z}) X_A$
 $X_B = 1$ then $Y_B = (\frac{z-1}{z}) Y_A$
 (if X_A yields Y_A , X_B yields Y_B .)
 $(\frac{z-1}{z}) = 1 - \frac{1}{z}$

1. If the final value to a unit step input to $G(z)$ is 5, then the final value to an IMPULSE input is:

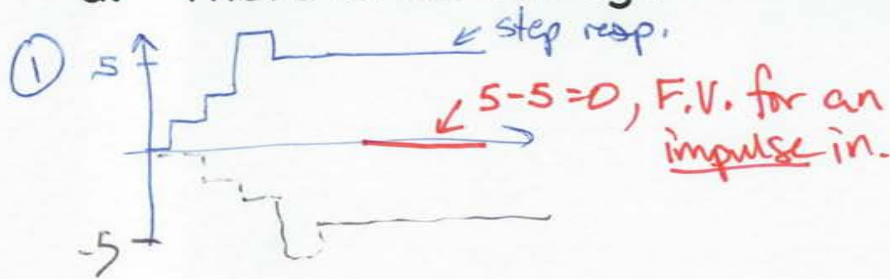
a. 5

b. 0

c. ∞

d. There is not enough information to determine this.

$$G(z) = \frac{Y(z)}{X(z)}, X(z) = \frac{z}{z-1}$$



X an impulse means
 $X_{tot} = 1$

$$X_1 + X_2 = X_{tot} = 1$$

$\uparrow X_2 = -\frac{1}{2}X_1$

Time shift & sign flip

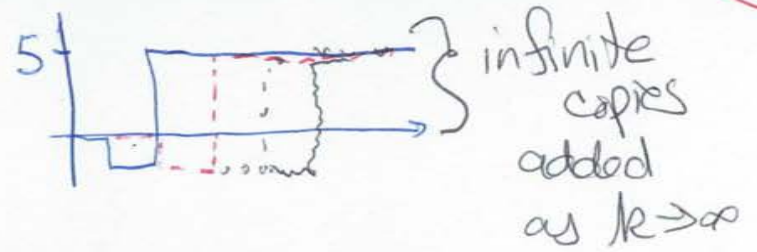
2. If the final value to an impulse input to $G(z)$ is 5, then the final value to a unit step input is:

a. 5

b. 0

c. $+\infty$

d. There is not enough information to determine this.



Pop Quiz!

3. The Final Value Theorem says:

a. Just blindly plug in "z=0", always.

b. Just blindly plug in "z=1", always.

c. Given transfer function $G(z)=Y(z)/X(z)$ has some input $X(z)$,

the final value of $Y(z)$ will be: $\lim_{z \rightarrow 1} \left(\frac{z-1}{z} X(z) \cdot G(z) \right)$

d. Use definition in "c.", but only apply IF POLES ARE STABLE!

this denominator doesn't matter.

For 1. & 2 (last page),

$$\lim_{z \rightarrow 1} \left(\frac{X_B(z)}{X_A(z)} \right) \cdot \text{F.V. of } Y_A(z) = \text{F.V. of } Y_B$$

otw., the "final value" is not well defined.

1. $X_A = \frac{z}{z-1}$ (step), $X_B = 1$ $\therefore \frac{X_B}{X_A} = \frac{z-1}{z}$ } goes to 0 as $z \rightarrow 1$

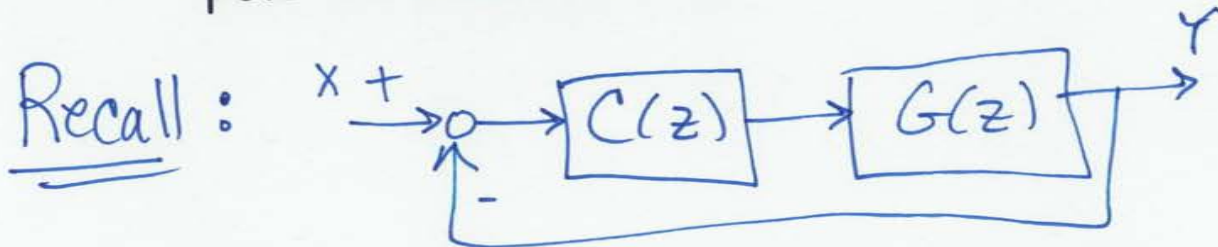
2. $X_A = 1$ (impulse), $X_B = \frac{z}{z-1}$ $\therefore \frac{X_B}{X_A} = \frac{z}{z-1}$ } goes to ∞ as $z \rightarrow 1$

$\uparrow$
 $z-1 \rightarrow 0$

Pop Quiz!

4. For "Direct Design" of controller $C(z)$ of an open-loop plant, $G(z)$, to yield some desired closed-loop plant, $P(z)$, which statements are TRUE:

- Yes! ✓ a. $P(z)$ cannot respond faster than $G(z)$, since $C(z)$ is causal.
 Yes! ✓ b. Zeros of $G(z)$ outside the unit circle cannot be "canceled" using poles of $C(z)$, since $C(z)$ can't have unstable poles.
 No. ✗ c. Unstable poles of $G(z)$ should just become zeros in $C(z)$, using "pole-zero cancellation".

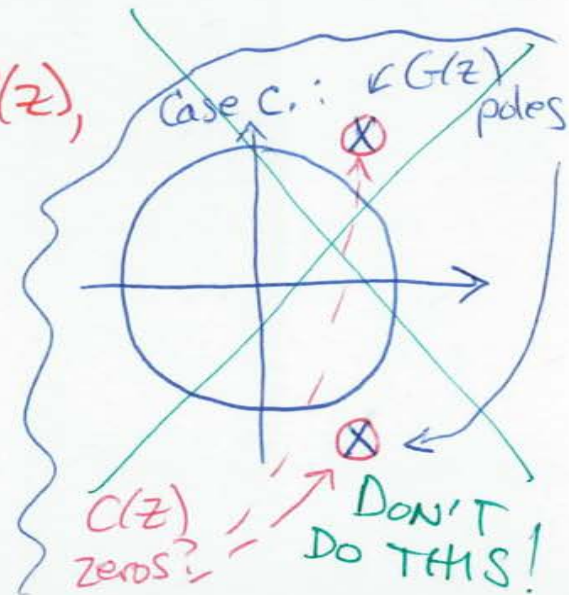


$$P(z) = \frac{Y(z)}{X(z)}$$

So, to get a desired $P(z)$,

$$P = \frac{CG}{1+CG} \quad \leftarrow \quad C = \frac{1}{G} \left(\frac{P}{1-P} \right)$$

Say $G(z)$ has unstable poles...
 We cannot just put zeros of C here to "cancel" them.



Direct Design: One last thing!

Example: $G(z) = \frac{z}{z^2 - 1.8z + \frac{9}{4}} = \frac{az^m + \dots}{bz^n + \dots}$

for an impulse input, $y(k=0)=0$
 $y(k=n-m) = \frac{a}{b}$

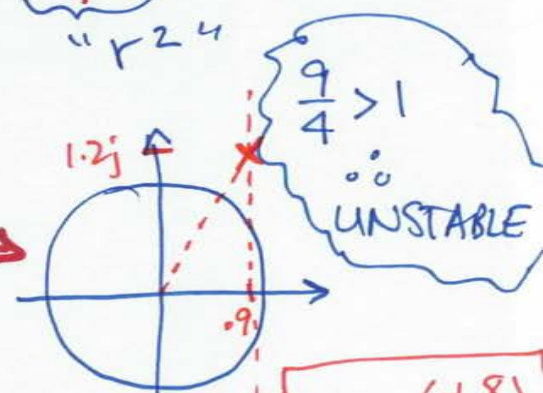
$\leftarrow$ so $y(k=1)=1$

" $-2x^4$ " " r^2 "

Open-loop poles of $G(z)$?

$$z = +0.9 \pm 1.2j$$

UNSTABLE



Instead of putting zeros of $C(z)$ "on top of" $G(z)$,

Let: $G = \frac{b(z)}{a(z)} = \frac{b}{a}$

$$C = \frac{c}{d}$$

$$P = \frac{e}{f}$$

So, $C = \frac{1}{G} \left(\frac{P}{1-P} \right)$

$$C = \frac{a}{b} \frac{e}{f-f-e}$$

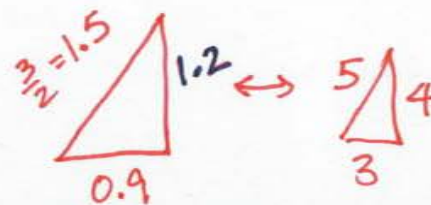
To "cancel out" a , we can let: $a = f - e$

So unstable poles of $G(z)$ become zeros of $1-P$.

$$\therefore 1-P = \frac{f}{f} - \frac{e}{f} = \frac{f-e}{f}$$

$$r^2 = \frac{9}{4}$$

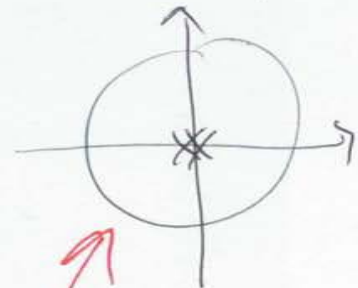
$$\therefore r = \frac{3}{2}$$



Say $G(z) = \frac{z}{(z^2 - 1.8z + \frac{9}{4})}$

∴ we want $P(z)$ w/ poles @ $z=0, z=0$.

" $z^2 = 0$ " ← char. eqn.



↑
Deadbeat
control
wanted.

$$P = \frac{e}{f}, C = \frac{c}{d}, G = \frac{b}{a}$$

Now, the zeros of $P(z)$ will be set using the "trick" on last page...

$$f = z^2$$

$$e = f - a = z^2 - (z^2 - 1.8z + \frac{9}{4})$$

$$\therefore e = 1.8z - \frac{9}{4}$$

$$C = \frac{\cancel{a}}{b} \cdot \frac{e}{\cancel{(f-a)}} = \frac{e}{b} = \boxed{\frac{1.8z - 2.25}{z} = C(z)}$$

cancel, by design.

State space: Block diagram of equations

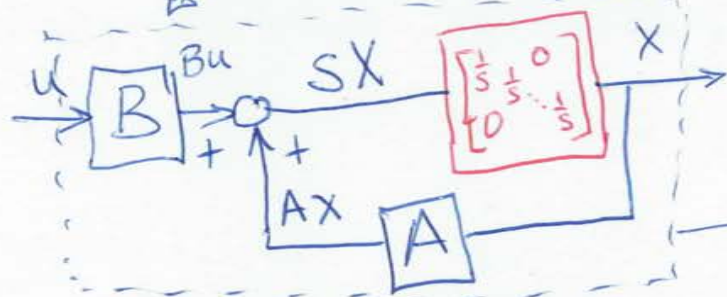
1. Dynamics. (What internal system does, "open loop".)

(DT case)

$$\underline{CT} \rightarrow \dot{X} = AX + Bu$$

$$sX = AX + Bu$$

$$\rightarrow \text{or } zX = A_d X + B_d u$$

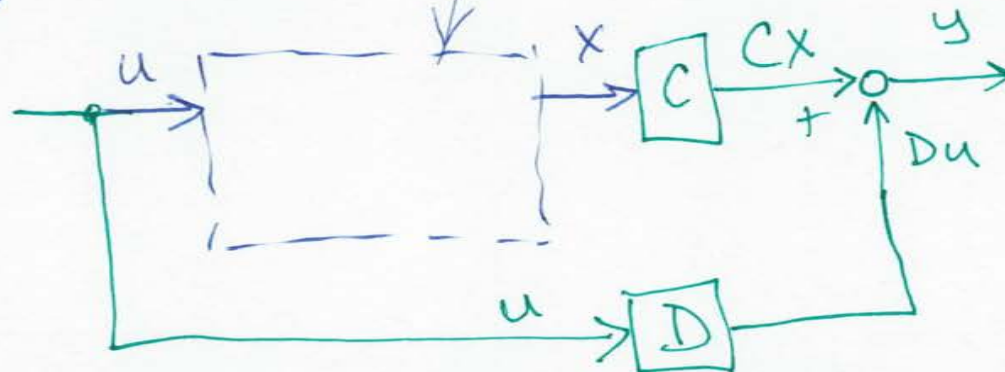


$$X = \left(\frac{1}{s} I\right) sX$$

} open-loop dynamics

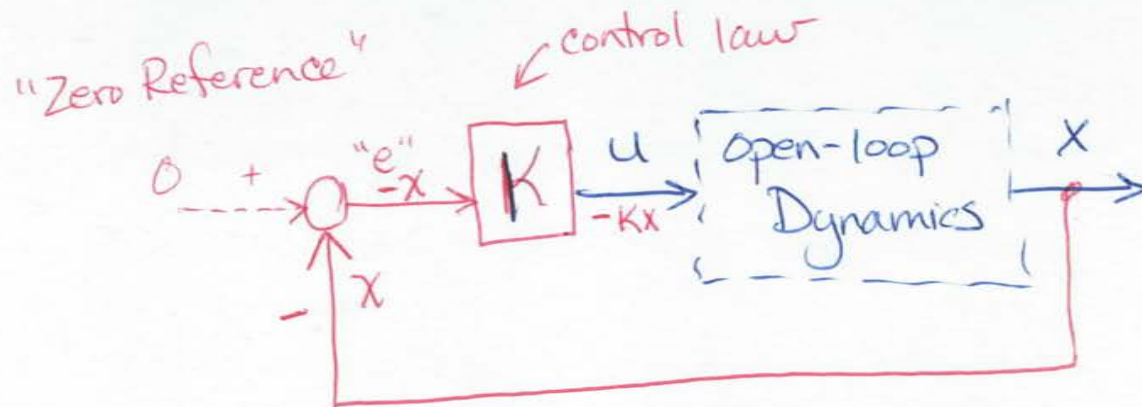
2. Outputs. (Things we can MEASURE.)

$$y = Cx + Du$$



State space: Block diagram of equations

- Control: A way to MODIFY the dynamics. i.e., set u as a function of X , via a "control law", e.g., a "PD controller" (for example)...



n : states
 m : outputs
 k : actuations

Control Law: $u = -KX$

$(k \times 1)$ $(k \times n)$ $(n \times 1)$

Consider

$$X = \begin{bmatrix} \dot{x} \\ x \end{bmatrix}$$

(2×1)

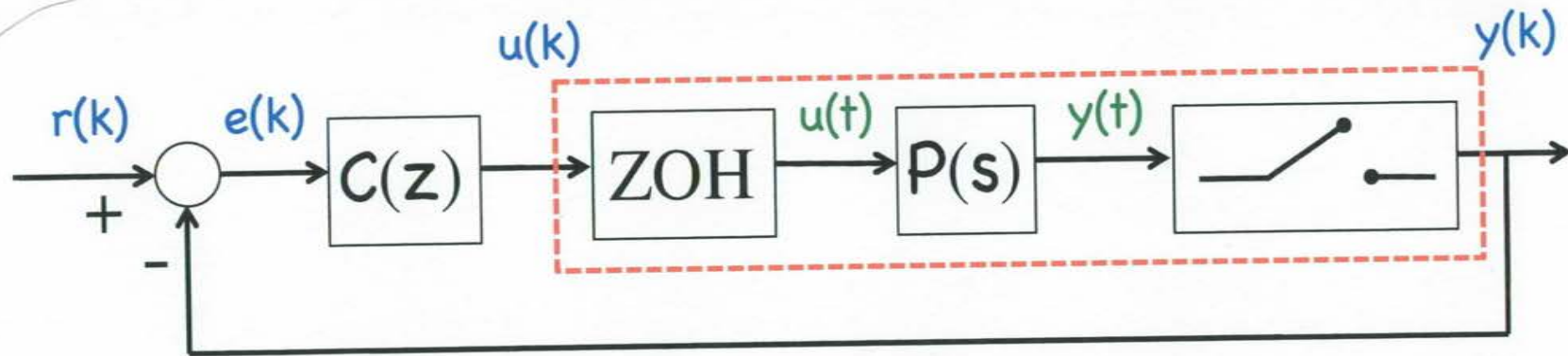
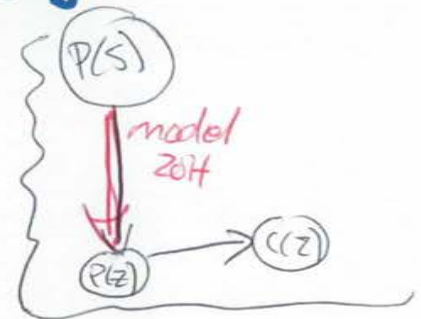
u some 1×1 (scalar) actuation

$\therefore K = [K_1, K_2]$
 $(k \times n)$
 (1×2)

$$\begin{aligned}
 u = -KX &= -K_1 \dot{x} - K_2 x \\
 &\quad \uparrow \quad \quad \uparrow \\
 &\quad x_1 = \dot{x} \quad x_2 = x \\
 &= -K_d \dot{x} - K_p x \\
 &\quad \quad \quad \text{a lot like PD!}
 \end{aligned}$$

"Case 2": Modeling the ZOH plus sampling

Given some C.T. system, with
 $A, B, C \text{ \& } D \dots$



$$A_d = e^{AT}$$

$$= \expm(AT) \neq \exp(AT)$$

"matrix exponential"

"↑ element by element"

$$B_d = \int_0^T e^{A(T-t)} dt B = A^{-1}(A_d - I)B$$

"Case 2": Modeling the ZOH plus sampling

The Matrix Exponential:

$$e^M = \sum_{k=0}^{\infty} \frac{1}{k!} M^k$$

Properties:

$$e^{M \times 0} = I$$

$$e^{M(s+t)} = e^{Ms} e^{Mt}$$

$$e^{-Mt} e^{Mt} = I$$

$$\frac{de^{Mt}}{dt} = M e^{Mt}$$

Example 1: $M=1$

(M just a 1x1 matrix, i.e., a scalar...)

$$e^1 = 1^0 + 1^1 + \frac{1}{2!} + \frac{1}{3!} + \dots \\ = 2.718281828 \text{ (etc...)}$$

Example 2: $\ddot{x} + 5\dot{x} + 10x = u$ ($T = 1\text{sec}$)

$$X = \begin{bmatrix} \dot{x} \\ x \end{bmatrix}, \quad \dot{X} = AX + Bu$$

$\ddot{x} = -5\dot{x} - 10x + u$

$\dot{x} = \dot{x}$ (?) $\leftarrow 0 \times u$

$\left(\frac{d}{dx} x_2 = x_1 \right)$

$$A = \begin{bmatrix} -5 & -10 \\ 1 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

In MATLAB: $\exp(A)$ vs $\expm(A)$?

Approximations, for "small T"...

Note: Analogous approximation trick applies for " e^{AT} " when "AT" has "small" entries as for " e^{sT} " when "sT" has small magnitude:

Example: $\ddot{x} + 2\dot{x} + 5x = u$ ($T = 0.01\text{sec}$)

If $X = \begin{bmatrix} \dot{x} \\ x \end{bmatrix}$, Then $A = \begin{bmatrix} -2 & -5 \\ 1 & 0 \end{bmatrix}$, $B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$
w/ zoh:

$$A_d = \expm(A \cdot 0.01) = \begin{bmatrix} .97995 & -.00495 \\ .0099 & .99975 \end{bmatrix}, B_d = ?$$

Similar to last page!

Forward Euler approximation:

$$A_d = I + AT$$

↑ for "small" T, zoh answer is "close" to this.

$$e \begin{bmatrix} A & B \\ 0 & 0 \end{bmatrix}^T = \begin{bmatrix} A_d & B_d \\ 0 & I \end{bmatrix}$$