

Today: Pole Placement

Lecture 12

ECE 147B

Digital Control

...for poles of the Controlled system dyn.

Reading: FPW 8.1
or: FV (9.1), 9.2

- Topics:
- ✓ Modeling the ZOH / Review from last time
 - ✓ State feedback: $u = -Kx$
 - ✓ Control Canonical Form
 - Pole Placement
 - Controllability

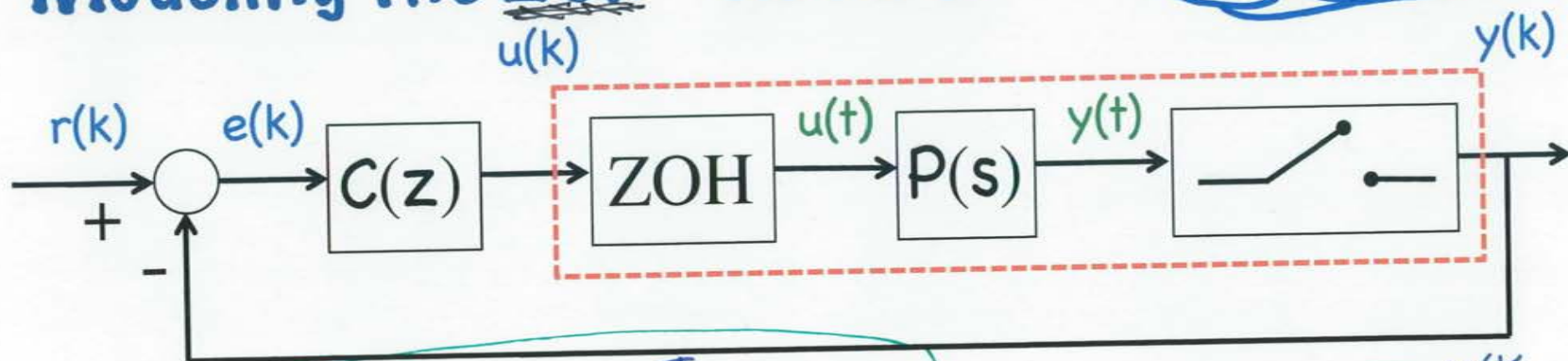
Next Time!

Next Class: Estimator design via pole placement.
- FPW 8.2.1-8.2.4 <or> FV 9.5.1, (RS-12)

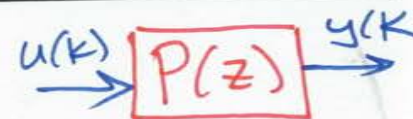
for poles of an observer, to estimate states.

Modeling the ZOH - REVIEW

Z.O.H. is the "Now-Menu" part



$$A_d \equiv e^{AT}, \quad B_d \equiv \int_0^T e^{At} dt B$$



The Matrix Exponential:

$$e^M = \sum_{k=0}^{\infty} \frac{1}{k!} M^k$$

expm command

...Can avoid this integral

A trick:

$$e^{\begin{bmatrix} A & B \\ 0 & 0 \end{bmatrix} T} = \begin{bmatrix} A_d & B_d \\ 0 & I \end{bmatrix}$$

"M"

Example: $\ddot{x} + 2\dot{x} + 5x = u$
($T = 0.01\text{sec}$)

$$\dot{X} = \begin{bmatrix} \dot{x} \\ x \end{bmatrix}, \quad A = \begin{bmatrix} -2 & -5 \\ 1 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

Forward Euler approximation:

$$A_d \approx \begin{bmatrix} .98 & -.05 \\ .01 & 1 \end{bmatrix}$$

$$A_d \approx I + AT, \quad B_d = BT$$

*e^M means $\text{expm}(M)$
[in MATLAB]*

Note that this is "Control canonical" form.

State space: Block diagram of equations

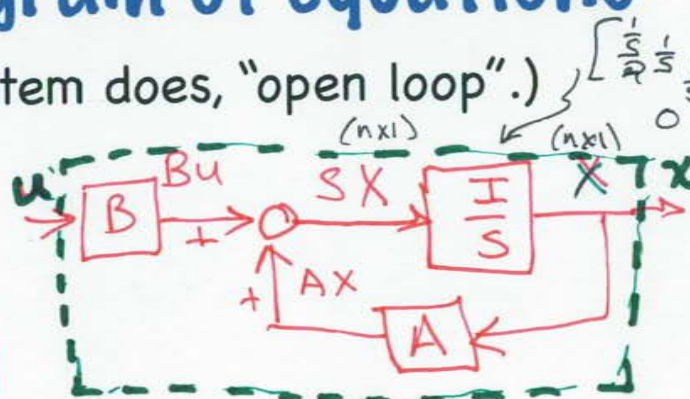
1. Dynamics. (What internal system does, "open loop".)

n states, (in x)

CT: $sX = AX + Bu$

Very analogous version for DT...

or $\rightarrow [zX = A_d X + B_d u]$



For SISO case:

$$P(z) = \frac{X(z)}{U(z)}$$

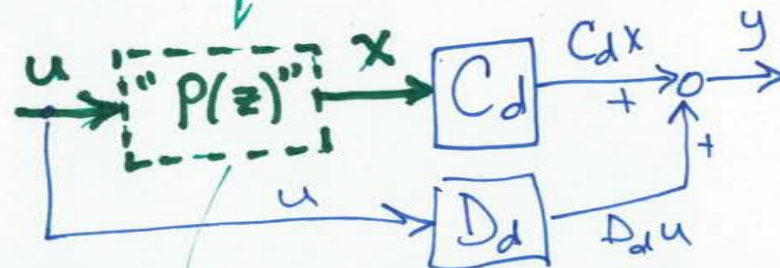
is inside the box.

2. Outputs. (Things we can MEASURE.)

k outputs, (in y)

CT: $y = Cx + Du$

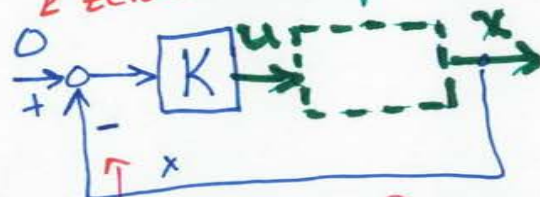
DT: $y = C_d X + D_d u$



3. Control: A way to MODIFY the dynamics, i.e., set u as a function of x , via a "control law", e.g., a "PD controller" (for example)...

m inputs (in u)

Note we have K zero as a reference (for each x state)



negative feedback.

closed-loop dynamics

$$u = -Kx$$

$$sX = AX + B(-Kx)$$

$$sX = (A - BK)x$$

A Review...

State space: Poles and Zeros

1. Dynamics. (What internal system does, "open loop".) → **POLES**
Solutions for $x \neq 0$, such that $u=0$? ← $u=0$. What $x(t)$ are still allowed?
 $sx = Ax + Bu$ $u=0$ ← $zx = A_d x + B_d u$
 $(sI - A)x = 0$
 $\therefore \boxed{\det(sI - A) = 0}$ ← Solutions are poles...
...and these are $\text{eig}(A)$.

2. Outputs. (Things we can MEASURE.) → **ZEROS**
Solutions for $u \neq 0$, such that $y=0$?
 $(sI - A)x = Bu$ $Y = Cx + Du$ $Y = C_d x + D_d u$
 $x = (sI - A)^{-1} Bu$
 $\therefore y = C(sI - A)^{-1} Bu + Du$
 $y = [C(sI - A)^{-1} B + D]u$
 $y=0$ when $0 = [C(sI - A)^{-1} B + D] \rightarrow \det[C(sI - A)^{-1} B + D] = 0$
Can write as... $\det \begin{bmatrix} sI - A & -B \\ C & D \end{bmatrix} = 0$
← solutions are the zeros.

State space: CLOSED-LOOP Poles (and Zeros)

3. Control: A way to MODIFY the dynamics. i.e., set u as a function of X , via a "control law", e.g., a "PD controller" (for example)...

State feedback:

$$u = -KX$$

$$X \equiv \begin{bmatrix} \dot{x} \\ x \end{bmatrix}$$

$$K_d \dot{x} + K_p x$$

$$KX = K_1 \dot{x} + K_2 x$$

$$sX = Ax + Bu = Ax - BKx$$

$$\rightarrow (sI - (A - BK))X = 0$$

$$\det[sI - (A - BK)] = 0$$

Solutions are closed-loop poles.

OR:

$$\text{eig}(A - BK)$$

$$zX = A_d x + B_d u = A_d x - B_d Kx$$

Same math...
... but "z-plane" meaning
for pole locations.

$$\det[zI - (A_d - B_d K)] = 0$$

i.e., "A" (open loop)
is replaced by
"A - BK"

State feedback example

$$\ddot{x}_2 + 2\dot{x}_2 + 5x_2 = 0$$

$$s^2 + 2s + 5 = 0$$

when $u=0$,
to find poles

We can "read off" the coefficients from A

$$m\ddot{x} + b\dot{x} + kx = f$$

$$X = \begin{bmatrix} \dot{x} \\ x \end{bmatrix}$$

$$K = [?]$$

- Say you are given the system dynamics and state variable definition at left.

($m=1$, $b=2$, $k=5$)

- What size must matrix "K" be? (1×2)
- * What values in K would result in closed loop poles with $\omega_n = 10$ (rad/s) and $\xi = 1$?

$$K = [K_1 \ K_2]$$

$$BK = \begin{bmatrix} K_1 & K_2 \\ 0 & 0 \end{bmatrix}$$

$$\ddot{X} = \frac{-b}{m}\dot{X} - \frac{k}{m}X + \frac{f}{m}$$

$$\dot{X} = \begin{bmatrix} \ddot{X} \\ \dot{X} \end{bmatrix} = AX + Bu$$

$$A = \begin{bmatrix} -2 & -5 \\ 1 & 0 \end{bmatrix}, B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$A = \begin{bmatrix} -\frac{b}{m} & -\frac{k}{m} \\ 1 & 0 \end{bmatrix}, B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$A - BK = \begin{bmatrix} -2-K_1 & -5-K_2 \\ 1 & 0 \end{bmatrix}$$

$$\therefore 2+K_1=20 \rightarrow K_1=18$$

$$5+K_2=100 \rightarrow K_2=95$$

$$\frac{d}{dt}x_1 = \dot{x}_2 = x_1$$

$$\ddot{x}_2 + \frac{b}{m}\dot{x}_2 + \frac{k}{m}x_2 = 0 \text{ (for } u=0)$$

* $\therefore$ We want: $s^2 + 2\zeta\omega_n s + \omega_n^2 = 0 \rightarrow s^2 + 20s + 100 = 0$

open loop dynamics:

$$s^n + a_1 s^{n-1} + a_2 s^{n-2} + \dots + a_n = 0$$

Roots are o.l. poles!

"Control Canonical Form"

Note:

① negative of the coefficients of the OPEN-LOOP characteristic eqn.

$$A = \begin{bmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & 1 & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$BK =$$

$$\begin{bmatrix} K_1 & K_2 & \dots & K_n \\ 0 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 0 \end{bmatrix}$$

$$K = [K_1 \ K_2 \ \dots \ K_{n-1} \ K_n]$$

② off-diagonal 1's:

$$\frac{d}{dt} X_p = X_{p-1}$$

$$X_p = \dot{X}_{p+1}$$

for $p > 1$, since no " X_0 " exists...

So, the states are related as derivatives of one another...

... And: X_1 is the highest derivative.

negative of the coefficients of the CLOSED-LOOP char. eqn.

$$A - BK =$$

$$\begin{bmatrix} -a_1 - K_1 & -a_2 - K_2 & \dots & -a_{n-1} - K_{n-1} & -a_n - K_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & 1 & 0 \end{bmatrix}$$

$$\begin{aligned} \dot{X}_2 &= X_1 \\ \dot{X}_3 &= X_2 \\ &\vdots \\ \dot{X}_n &= X_{n-1} \end{aligned}$$

For "control canonical" form

Roots are closed-loop poles

$$s^n + (a_1 + K_1)s^{n-1} + (a_2 + K_2)s^{n-2} + \dots + (a_n + K_n) = 0$$

"Control Canonical Form"

$$B = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

One input, which affects only $\dot{x}_1$
 $(\frac{d^n}{dt^n} x_n) \leftarrow \dot{x}_1 = \ddot{x}_2 = \ddot{x}_3$

Example: 3rd order:
 3 states,
 3 poles,
 (3 values in K .)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -a_1 & -a_2 & -a_3 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

$$A - BK = A - \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} [K_1 \ K_2 \ K_3]$$

closed-loop dynamics:

$$\dot{x}_1 = -(a_1 + K_1)x_1 - (a_2 + K_2)x_2 - (a_3 + K_3)x_3$$

$$\begin{bmatrix} -a_1 - K_1 & -a_2 - K_2 & -a_3 - K_3 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$

$\dot{x}_2 = x_1$
 $\dot{x}_3 = x_2$
 $\ddot{x}_3 = \ddot{x}_2 = \ddot{x}_1$
 $\therefore \ddot{x} = \begin{bmatrix} \ddot{x} \\ \dot{x} \\ x \end{bmatrix}$

So, the char. eqn. is:

$$(\ddot{x}_1 = \ddot{x} = -(a_1 + K_1)\ddot{x} - (a_2 + K_2)\dot{x} - (a_3 + K_3)x)$$

$$s^3 + (a_1 + K_1)s^2 + (a_2 + K_2)s + (a_3 + K_3) = 0$$

↑ unchanged

"Control Canonical Form"

Canonical Form makes it "easy" to solve for $K \dots$

Example:

$$\underline{A} = \begin{bmatrix} 3 & -5 \\ 1 & 0 \end{bmatrix} \quad \underline{B} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

For state feedback control " $u = -Kx$ ", solve for K such that closed-loop poles are at $s = -3, s = -3$.

↓

$$(s+3)(s+3) = 0$$

$$s^2 + 6s + 9 = 0$$

$$A - BK = \begin{bmatrix} 3 - K_1 & -5 - K_2 \\ 1 & 0 \end{bmatrix}$$

$$s^2 - (3 - K_1)s + (5 + K_2) = 0 \leftarrow \text{closed loop.}$$

$$K_1 - 3 = 6 \rightarrow \boxed{\therefore K_1 = 9}$$

$$5 + K_2 = 9 \rightarrow \boxed{\therefore K_2 = 4}$$

... once a desired char. eqn. for the closed-loop system is known.

NOT

Control Canonical Form

Example:

$$A = \begin{bmatrix} 0 & 1 \\ -5 & 3 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

still off-diagonal ones!

Note order is FLIPPED!

$$\begin{aligned} \dot{x} &= \dot{x}_1 = x_2, & x &= x_1 \\ \ddot{x} &= \dot{x}_2 = -5x_1 + 3x_2 + u \\ \ddot{x} &= -5x + 3\dot{x} + u \\ \ddot{x} - 3\dot{x} + 5x &= u \end{aligned}$$

For state feedback control " $u = -Kx$ ", solve for K such that closed-loop poles are at $s = -3, s = -3$. HINT: Same dynamics but different definition of " x " here!

* Although this is NOT "control canonical" form, it is very similar...

Gain matrix still defined as: $K = [K_1, K_2]$

Punchline:

Negative values of

of char. eqn.

* Coefficients are still entries in the A matrix...

But order they are listed is FLIPPED!

So, K is also FLIPPED!

$K_1 = 4, K_2 = 9$

"Control Canonical Form"

Example:

$$A_d = \begin{bmatrix} 0.6 & -1.2 \\ 1 & 0 \end{bmatrix} \quad B_d = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

For state feedback control " $u = -Kx$ ", solve for K such that closed-loop poles are at $z=0, z=0$. This is "deadbeat" control!

$$zX = A_d X + B_d u$$

$$\begin{cases} zX_1 = 0.6X_1 - 1.2X_2 + u \\ zX_2 = X_1 \end{cases}$$

$$zX_1 = z^2 X_2 = 0.6 zX_2 - 1.2 X_2 + u$$

$$z^2 X_2 - 0.6 zX_2 + 1.2 X_2 = u$$

For n^{th} -order system, characteristic eqn. is wrt X_n (the last element in X).

$$z^2 + (-0.6 + K_1)z + (1.2 + K_2) = 0$$

$$\therefore z^2 = 0 \text{ REQUIRES } K_1 = 0.6, K_2 = -1.2$$

Same holds in the discrete-time (DT) case...

In Control Canonical form,

$$\begin{aligned} zX_2 &= X_1 \\ zX_3 &= X_2 \\ &\vdots \\ zX_n &= X_{n-1} \end{aligned}$$

$$X_2(k+1) = X_1(k)$$

$$X_3(k+1) = X_2(k)$$

$$\vdots$$

$$X_n(k+1) = X_{n-1}(k)$$

$$\text{So, } X_1(k) = X_2(k+1) = X_3(k+2) = \dots = X_n(k+n-1)$$

All states are interrelated via the "Z" operator (time delay).

w/ $u = -Kx$,
char. eqn. is...

Pole Placement

NEXT CLASS

Comments:

1. By now, you should see (intuitively) how to solve for K such that " $\text{eig}(A-BK)$ " [or " $\text{eig}(A_d-B_dK)$ "] yield desired poles...
2. But our hand calculations would be **TEDIOUS** for large-dimensional, MIMO (multi-input multi-output) systems!

Is there a more efficient solution? → YES! This is "pole placement".

First, let's look at how to do this IN MATLAB:

```
A = rand(4,4); % some random, 4th-order open-loop system dynamics...
B = rand(4,1); % ...including actuator inputs.
pdes = [-1 -2 -3 -4]; % desired poles (4 poles; 4th-order system...)
pnow = eig(A) % open-loop poles
K = place(A,B,pdes) % "pole placement" command in matlab
```

```
K2 = acker(A,B,pdes) % alternate "pole placement" command
```

```
pact = eig(A-B*K) % ACTUAL closed-loop poles!
```

Controllability

NEXT CLASS

Given matrices A and B (for CT), or given A_d and B_d (for DT), the CONTROLLABILITY matrix is defined as:

$$C \equiv [B, AB, A^2B, \dots, A^{n-1}B]$$

The system is CONTROLLABLE if and only if this matrix has FULL RANK (meaning it is INVERTIBLE).

Note the CHARACTERISTIC EQUATION for your desired CLOSED-LOOP (still nth-order) dynamics can be written as:

$$z^n + \alpha_1 z^{n-1} + \alpha_2 z^{n-2} + \dots + \alpha_n$$

Then, the GAIN MATRIX "K" needed will be: $K = [0 \dots 0, 1] C^{-1} \alpha_c(A)$

Where $\alpha_c(A) \equiv A^n + \alpha_1 A^{n-1} + \alpha_2 A^{n-2} + \dots + \alpha_n I$