

Today: Reduced-Order Estimators

Lecture 15

ECE 147B
Digital Control

Reading: FPW 8.2.5, 8.3
or: FV 9.5.2, 9.6 (RS-13)

Topics:

- Separation Principle
- Guidelines for pole placement (control and est.)
- Reduced-Order Estimator
- Frequency Response Methods

Next Class: Frequency Response Methods.
- FPW 7.4 <or> FV (6.4), 6.5, (6.6) (RS-1)

Homework 6 : Due Tues
(in class).

Using the state estimate for feedback...

Recall STATE FEEDBACK
Control uses the true state:

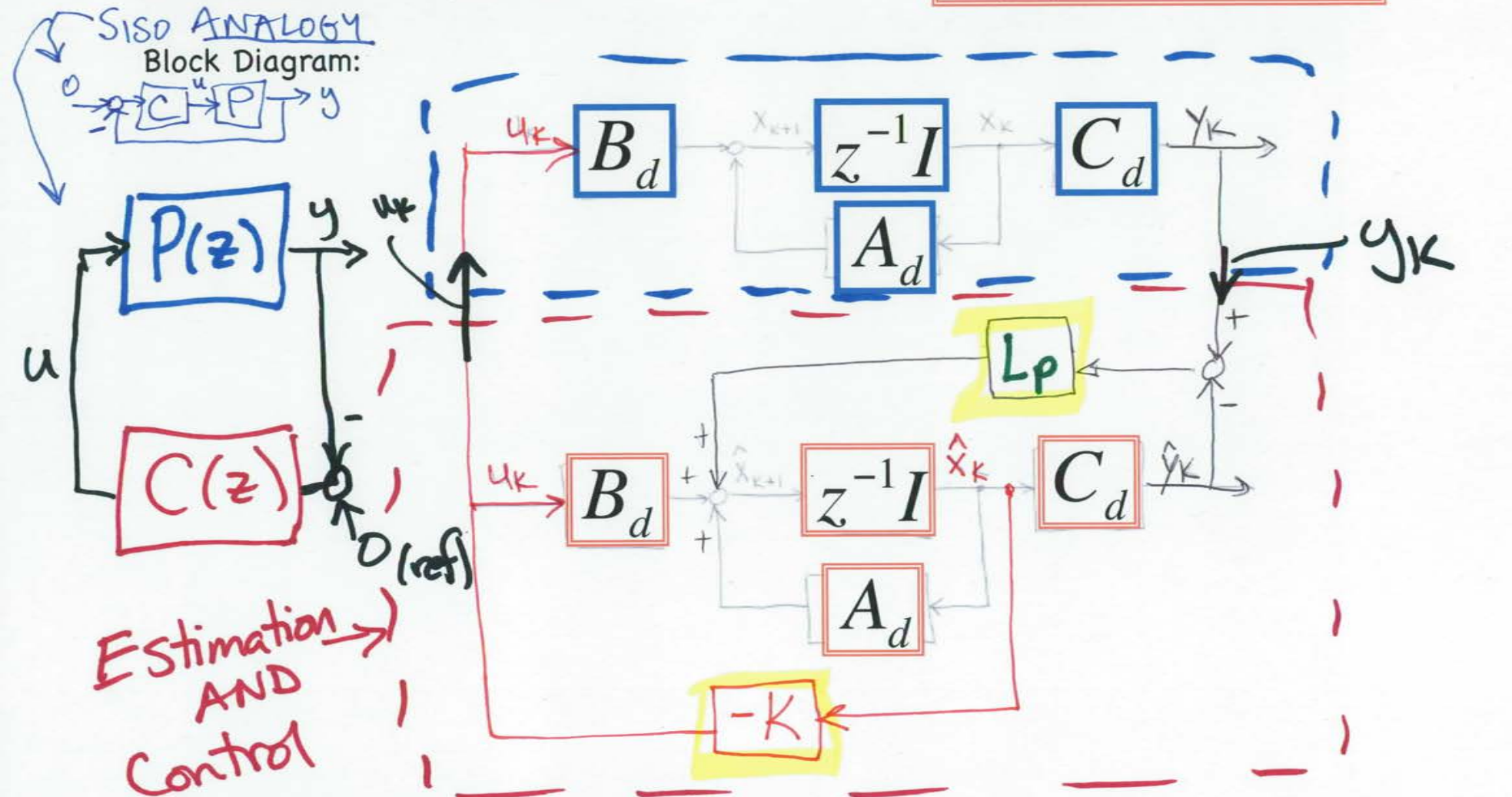
$$u(k) = -Kx(k)$$

estimate

What if we use the state ESTIMATE
for feedback control, instead?

$$u(k) = -K\hat{x}(k)$$

SISO ANALOGY
Block Diagram:



Closed-loop Dynamics, for state (x) and error (e_x)

MATRIX form for DYNAMICS: for STATES $\hat{x}$ ERRORS in states.

eigenvalues?

$$\begin{bmatrix} x_{k+1} \\ e_{k+1} \end{bmatrix} = \begin{bmatrix} (A - BK) & BK \\ 0 & (A - LC) \end{bmatrix} \begin{bmatrix} x_k \\ e_k \end{bmatrix}$$

$(e = x - \hat{x})$ (n x n) "M"

$\cdot (eig(A - BK), eig(A - LC))$
 $\uparrow$ 2n poles, determined "separately"

NOTE - Matrix above has "Upper Block Diagonal" form. Examples:

n=1 (state)

$$\det \left(\begin{bmatrix} z & 0 \\ 0 & z \end{bmatrix} - \begin{bmatrix} a & c \\ 0 & b \end{bmatrix} \right) = 0$$

$\uparrow \det(zI - M)$, M is $\begin{bmatrix} a & c \\ 0 & b \end{bmatrix}$

$$\det \begin{bmatrix} z-a & -c \\ 0 & z-b \end{bmatrix} = 0 = (z-a)(z-b) + 0 = 0$$

$\begin{bmatrix} z=a \\ z=b \end{bmatrix} \leftarrow \text{poles}$

n=2

$$\det \begin{bmatrix} z & 0 & 0 & 0 \\ 0 & z & 0 & 0 \\ 0 & 0 & z & 0 \\ 0 & 0 & 0 & z \end{bmatrix} - \begin{bmatrix} a_1 & a_2 & c_1 & c_2 \\ a_3 & a_4 & c_3 & c_4 \\ 0 & 0 & b_1 & b_2 \\ 0 & 0 & b_3 & b_4 \end{bmatrix} = 0$$

"D" = 0 (n x n)
 "A" (n x n)
 "B" (n x n)

"C" (n x n) $eig(M) \rightarrow \det(zI - M) = 0$

are the SAME as:
 $(eig(A), eig(B))$
 ($\hat{A}$ & $\hat{B}$ as defined at left!)

does NOT depend of "C" b/c "D" = 0

Eigenvalue examples, via MATLAB

Below is code to "see" some of the ideas for yourself - at least for our toy examples:

syms a1 a2 a3 a4 b1 b2 b3 b4 c1 c2 c3 c4 z - symbolic toolbox (in MATLAB)

```
A = [a1 a2; a3 a4];
B = [b1 b2; b3 b4];
C = [c1 c2; c3 c4];
```

```
M = [A C; zeros(2,2) B]
M =
```

```
[ a1, a2, c1, c2]
[ a3, a4, c3, c4]
[  0,  0, b1, b2]
[  0,  0, b3, b4]
```

```
zI = z*eye(4)
```

```
zI =
[ z, 0, 0, 0]
[ 0, z, 0, 0]
[ 0, 0, z, 0]
[ 0, 0, 0, z]
```

$$\det \begin{pmatrix} \begin{bmatrix} z & 0 & 0 & 0 \\ 0 & z & 0 & 0 \\ 0 & 0 & z & 0 \\ 0 & 0 & 0 & z \end{bmatrix} - \begin{bmatrix} a_1 & a_2 & c_1 & c_2 \\ a_3 & a_4 & c_3 & c_4 \\ 0 & 0 & b_1 & b_2 \\ 0 & 0 & b_3 & b_4 \end{bmatrix} \end{pmatrix} = \det(zI - M) = 0$$

$A = \begin{bmatrix} a_1 & a_2 \\ a_3 & a_4 \end{bmatrix}$
etc.

(2n x 2n)
w/ lower-left
(n x n) part
ALL ZEROS

```
det(zI-M)
```

```
ans =
```

```
z^4 - a4*z^3 - b1*z^3 - b4*z^3 - a1*z^3 + a1*a4*z^2 - a2*a3*z^2 + a1*b1*z^2 + a1*b4*z^2
+ a4*b1*z^2 + a4*b4*z^2 + b1*b4*z^2 - b2*b3*z^2 + a1*a4*b1*b4 - a1*a4*b2*b3 -
a2*a3*b1*b4 + a2*a3*b2*b3 - a1*a4*b1*z + a2*a3*b1*z - a1*a4*b4*z + a2*a3*b4*z -
a1*b1*b4*z + a1*b2*b3*z - a4*b1*b4*z + a4*b2*b3*z
```

```
simplify(det(zI-M))
```

```
ans =
```

```
(a2*a3 - a1*a4 + a1*z + a4*z - z^2)*(b2*b3 - b1*b4 + b1*z + b4*z - z^2)
```

= 0 (to find POLES)

Solvefor: this part = 0

this part = 0, separately.

Separation Principle

For feedback with an ESTIMATOR,

"open-loop" dynamics = feedback part

$$\hat{X}_{k+1} = A \hat{X}_k + B u_k + L_p (y_k - C \hat{X}_k)$$
$$u_k = -K \hat{X}_k \leftarrow \text{uses } \hat{X}_k \text{ NOT } X_k.$$

- 1) CONTROL for nth-order system has n poles, determined by $\text{eig}(A-BK)$.

Pick (dominant) closed-loop poles, e.g.,
via "pole placement", for " $\text{eig}(A-BK)$ "
↖ poles

- 2) ESTIMATION of n states results in another n poles, determined by $\text{eig}(A-LC)$ ← estimator poles.
Then, pick estimator poles (NOT dominant),
Generally (about) 2x - 4x "faster" than controller poles

- 3) TOTAL system now has 2*n poles:

∴ they are the union of $\text{eig}(A-BK)$
and $\text{eig}(A-L_p C)$
i.e., these are 2 SEPARATE (uncoupled) problems!

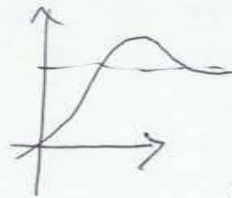
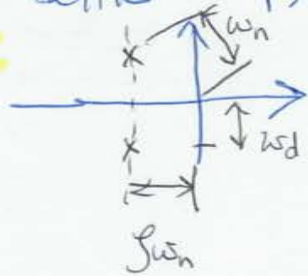
How to place poles, to set "K" and **Lp**?

$\therefore$ "2x-4x" faster than $\text{eig}(A-BK)$
 $\therefore \text{eig}(A-LC)$

Controller poles:

- ① Use classical control design specifications: ($\omega_d, t_{\text{rise}}, t_{\text{settle}}, M_p$, etc...) to pick "good" C.L. poles

S-plane



$$t_p = \frac{\pi}{\omega_d}$$

$$M_p = e^{-t_p/\tau}$$

$$\sigma = \zeta\omega_n$$

$$\tau = \frac{1}{\sigma}$$

Z-plane

$$z = e^{sT}$$

Then use "place" or "acker"...

Estimator poles:

- ② - Faster than control poles, so controlled CL poles dominate

Effects of Noise?

" $L y(k)$ " is INSTEAD " $L(y(k) + w(k))$ " BUT state dynamics (x) "see" both $(A-BK)$ and $(A-LC)$ poles.

$$\begin{bmatrix} x_{k+1} \\ e_{k+1} \end{bmatrix} = \begin{bmatrix} (A-BK) & BK \\ 0 & (A-LC) \end{bmatrix} \begin{bmatrix} x_k \\ e_k \end{bmatrix} + \begin{bmatrix} 0 \\ -L \end{bmatrix} n_k$$

$$e_{k+1} = (A-LC)e_k + L n_k$$

$$e \equiv x - \hat{x}$$

$$e_{k+1} = A(x_k - \hat{x}_k) - L(Cx_k - C\hat{x}_k + n_k)$$

$$e_{k+1} = Ae_k - LCe_k - Ln_k = (A-LC)e_k - Ln_k$$

$$\begin{aligned} x_{k+1} &= Ax_k + Bu_k \\ \hat{x}_{k+1} &= A\hat{x}_k + Bu_k + L(y_k + n_k - \hat{y}_k) \end{aligned}$$



∴ Making est. poles TOO FAST makes L LARGE → sensitive to noise!

Example: control and estimation, w/ MATLAB

CT dynamics

$$A = \begin{bmatrix} -1 & -1 \\ 1 & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

Control canonical form!

$$A - BK = \begin{bmatrix} -1 - K_1 & -1 - K_2 \\ 1 & 0 \end{bmatrix}$$

Negative of THIS we want to equal THAT.

Desired closed-loop poles

$$p_{ct} = [-10 + 10j, -10 - 10j]$$

WANTED: $s^2 + 20s + 200 = 0$

$$K_1 + 1 = 20$$

$$K_1 = 19$$

$$K_2 = 199$$

CT (continuous time) - n states (x), m inputs (u), l outputs (y)

DT (discrete time), $[T = 0.01 \text{ sec}]$ - system resulting from ZOH

$$M = \text{expm}([A, B; \text{zeros}(m, n+m)] * T)$$

$$A_d = M(1:n, 1:n);$$

$$B_d = M(1:n, n+1:\text{end});$$

" $z = e^{sT}$ "

$$pdt = \exp(pct * T);$$

$$A_d \approx \begin{bmatrix} .99 & -.01 \\ .01 & 1.0 \end{bmatrix}, B_d \approx \begin{bmatrix} .01 \\ 0 \end{bmatrix}$$

$$K_d = \text{place}(A_d, B_d, pdt)$$

$$K_d = [18.12, 180.88]$$

"Trick" to get A_d & B_d for ZOH (plus sampling) DT system

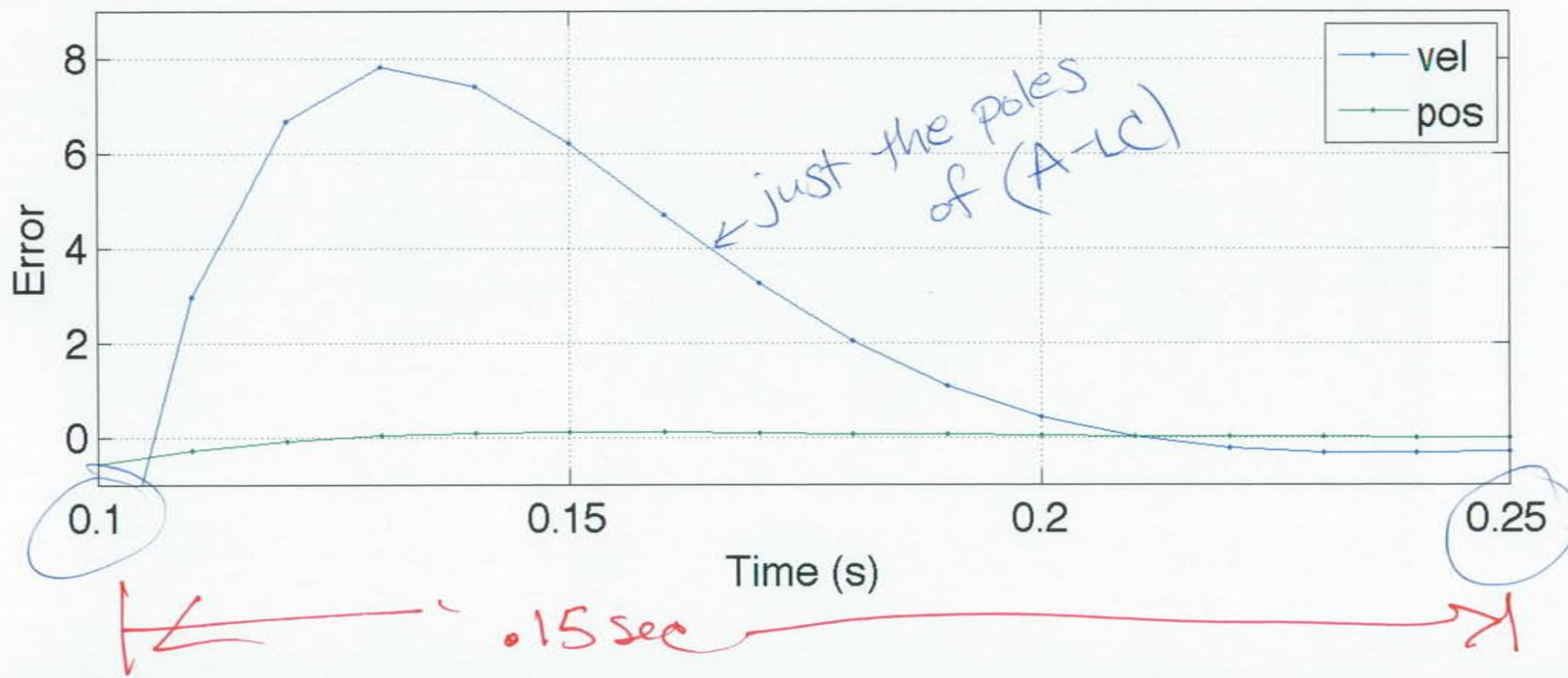
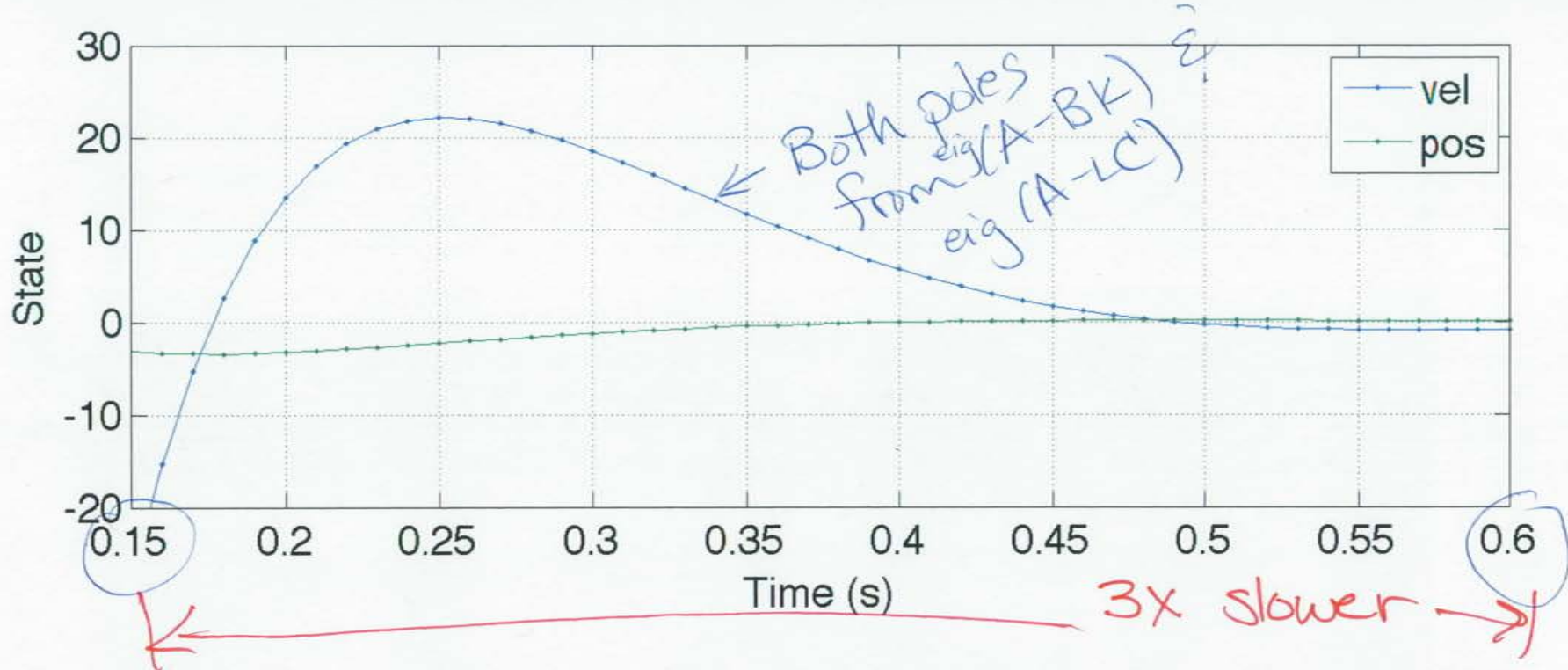
$$K = [K_1, K_2]$$

$$K = [19, 199]$$

CT dynamics

OR, use "c2d"

Not QUITE the same, but close.



Reduced-order Estimator

What if you only want to "estimate" a subset of the entire state vector? e.g., You only want to estimate "unmeasured" states, which are not inside y . For example, in LAB:

Position: encoder - measured, x

Velocity: Not measured! $\leftarrow$ unmeasured, $\dot{x}$

Let's partition the states, $x(k) = \begin{bmatrix} x_a(k) \\ x_b(k) \end{bmatrix}$ a : directly measured
 b : not measured $\leftarrow$ only estimate $\hat{x}_b$ w/ red-ord. est.

we will get this directly from measurement

$$\begin{bmatrix} x_a(k+1) \\ x_b(k+1) \end{bmatrix} = \underbrace{\begin{bmatrix} A_{aa} & A_{ab} \\ A_{ba} & A_{bb} \end{bmatrix}}_A \begin{bmatrix} x_a(k) \\ x_b(k) \end{bmatrix} + \underbrace{\begin{bmatrix} B_a \\ B_b \end{bmatrix}}_B u(k)$$

$\begin{matrix} \text{"}x_{k+1}\text{"} & & & \end{matrix}$

$$\boxed{\#1} \quad \underbrace{x_b(k+1)}_{\text{unknown}} = \underbrace{A_{bb} x_b(k)}_{\text{unknown}} + \underbrace{(A_{ba} x_a(k) + B_b u(k))}_{\text{known}}$$

Error dynamics

$\boxed{\#2} \rightarrow$ write an eqn for $\hat{x}_b(k+1) \dots \hat{\epsilon}$ then $\boxed{\#3}$ is calculate by $\boxed{\#1}$ minus $\boxed{\#2}$

Reduced-order Estimator

from last page

$$* \quad X_a(k+1) = A_{aa}x_a(k) + A_{ab}x_b(k) + B_a u(k)$$

This looks a lot like

$$x(k+1) = Ax(k) + Bu(k)$$

$$y(k) = Cx(k) + Du(k)$$

Think of this as "Cx" in "y=Cx"

$$\begin{aligned} \textcircled{1} \quad x_b(k+1) &= A_{bb}x_b(k) + (A_{ba}x_a(k) + B_b u(k)) \\ \textcircled{4} \quad (x_a(k+1) - A_{aa}x_a(k) - B_a u(k)) &= A_{ab}x_b(k) \end{aligned}$$

↑ "y(k)" = $\textcircled{3} \quad Cx(k)$

...if we make the following SUBSTITUTIONS:

Was → Now

- 1) $\textcircled{1} \quad x(k) \rightarrow x_b(k) \leftarrow$ States TO BE ESTIMATED
 - 2) $\textcircled{2} \quad A \rightarrow A_{bb} \leftarrow$ a sub-part of the full "A" matrix.
 - 3) $\textcircled{3} \quad Bu(k) \rightarrow (A_{ba}x_a(k) + B_b u(k)) \leftarrow$ "Known" inputs now include BOTH "Bu" and also terms depending on $x_a(k)$ [known/measured].
 - 4) $\textcircled{4} \quad y(k) \rightarrow (x_a(k+1) - A_{aa}x_a(k) - B_a u(k)) \leftarrow$
 - 5) $\textcircled{5} \quad C \rightarrow A_{ab} \leftarrow$ " $A_{ab}x_b(k)$ " is now analogous to "Cx"
- What is left on LHS of * once " $A_{ab}x_b(k)$ " (like "Cx") is moved to RHS

GOAL is to match THIS form:
(But estimate ONLY $x_b(k)$...)

$$\hat{x}(k+1) = A\hat{x}(k) + Bu(k) + L(y(k) - C\hat{x}(k))$$

Use piece $\textcircled{1}$ through $\textcircled{5}$ above!

Reduced-order Estimator

$$\hat{x}(k+1) = A\hat{x}(k) + Bu(k) + L(y(k) - C\hat{x}(k))$$

Traditional (not "reduced") form, which we wish to match.

#2 $\hat{x}_b(k+1) = \underline{A_{bb}}\hat{x}_b(k) + (\underline{A_{ba}x_a(k)} + \underline{B_b u(k)}) + L_r(\underbrace{[x_a(k+1) - A_{aa}x_a(k) - B_a u(k)]}_{\text{Uh oh!}} - \underbrace{A_{ab}\hat{x}_b(k)}_{= A_{ab}x_b(k)})$

We have a new estimator equation, as desired, but there is a PROBLEM! We do not have access to " $x_a(k+1)$ " yet! (Causality...)
(To be discussed NEXT PAGE...)

Recall:

#1 $x_b(k+1) = \underline{A_{bb}}x_b(k) + (\underline{A_{ba}x_a(k)} + \underline{B_b u(k)})$

So, use "place" with
"A" = A_{bb}
"C" = A_{ab}

Error Dynamics? $e_{xb} \equiv x_b - \hat{x}_b$, So, take #1 minus #2

$$x_b(k+1) - \hat{x}_b(k+1) = A_{bb}(x_b(k) - \hat{x}_b(k)) - L_r(A_{ab}x_b(k) - A_{ab}\hat{x}_b(k))$$

$\therefore e_b(k+1) = [A_{bb} - L_r A_{ab}]e_b(k)$ ← poles set by " $A_{bb} - L_r A_{ab}$ "

