

```

% Example of AUTOMATED GENERATION OF LAGRANGIAN EOM
%
% Note: This file requires the shareware function "fulldiff.m"
% to do chain rule for time derivatives.
%
% Example system:
%
%      _____|          | g (gravity)
%      |-----| -| b (damper)  \|/
%      |-----:          v
%      |          [m] (mass)  - - - -
%      |          <          :
%      | (constant > k (spring)  dm (rel displace of mass)
%      | arm length) <          :
%      |      La  _____ - - - -
%      |      |----- alpha, tau (acting wrt inertial frame on alpha)
%      |----- - - - -
%
% Process
% =====
%
% 0. Clear workspace (desirable):
clear all
format compact % more readable when single-spaced
%
% 1. Declare constant and variable symbolically.
syms m k b alpha dm g La tau
%
% 2. Define INDEPENDENT and COMPLETE set of Generalized Coordinates.
GC = {alpha, dm} % note CURLY BRACKET notation here and elsewhere!!
%
% 3. Define any DEPENDENT variables that are convenient. (For example,
% we may wish to define potential energy in terms of absolute height.)
xm = La*cos(alpha) % absolute x position of center of mass (COM)
ym = La*sin(alpha) + dm % absolute height of COM
%
% 4. Define TIME DERIVATIVES of the dependent variables:
dxm = fulldiff(xm,GC) % input arg GC are the independent vars of time
dym = fulldiff(ym,GC)
ddm = fulldiff(dm,GC)
for n=1:length(GC)
    dGC{n} = fulldiff(GC{n},GC)
end
%
% 5. Write expressions for...
% a. T* (kinetic energy):
Tstar = (1/2)*m*(dxm^2 + dym^2)
% b. V (potential energy):
V = m*g*ym + (1/2)*k*dm^2
% c. L = Tstar - V, except "L" might already be defined previously
Lagran = Tstar - V

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% 6. For each GC, calculate LHS of EOM:
%   d/dt(partial L wrt dxi_n) - (partial L wrt xi_n)
for n=1:length(GC)
    LHS{n} = fulldiff(diff(Lagran,dGC{n}),GC) - diff(Lagran,GC{n})
end

% 7. Define NON-CONSERVATIVE forces (or torque) for RHS of each EOM:
RHS{1} = tau;      % absolute torque on alpha DOF
RHS{2} = -b*ddm;   % damping force; dm is a relative coordinate

% 8. Print equations nicely on screen!
for n=1:length(GC)
    fprintf('\n__Equation %d:__\n',n)
    pretty(simplify(LHS{n})) % simplify, then print in "pretty" way...
    fprintf('  equals\n')
    pretty(simplify(RHS{n}))
    latex_output{n} = [latex(simplify(LHS{n})), ' = ', ...
        latex(simplify(RHS{n}))]; % to print in LATEX
end

% Now, the contents of latex_output{1} and latex_output{2} can be
% copied into your favorite LaTeX editor. To display nicely will
% still require some "hand editing" without latex, however!

```

Auto-Generation of Equations of Motion Example, in L^AT_EX

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Abstract

This example equation comes from the output to m-file eom_4bar_example.

1 MATLAB auto-formatting for EOMs

By default, MATLAB's `latex` function tends to display many variables in a non-*italic* Roman font which is not pleasing to the eye, nor easy to read. Below are our two equations of motion for the 4-bar spring-mass-damper system, for example.

The first EOM MATLAB generates is:

```
\mathrm{La}\, , m\, , \left(\mathrm{La}\, , \mathrm{d2alpha} + \mathrm{d2dm}\, ,
\cos\!\left(\mathrm{alpha}\right) + g\, ,
\cos\!\left(\mathrm{alpha}\right)\right) = \mathrm{tau}
```

In latex formatting, this becomes:

$$La\, m\, (La\, d2alpha + d2dm\, \cos(\alpha) + g\, \cos(\alpha)) = \tau \quad (1)$$

Similarly, the second equation output from MATLAB is:

```
- \mathrm{La}\, , m\, , \sin\!\left(\mathrm{alpha}\right)\, ,
{\mathrm{dalpha}}^2 + \mathrm{dm}\, , k + \mathrm{d2dm}\, ,
m + g\, , m + \mathrm{La}\, , \mathrm{d2alpha}\, , m\, ,
\cos\!\left(\mathrm{alpha}\right) = - b\, , \mathrm{ddm}
```

which becomes:

$$-La\, m\, \sin(\alpha)\, d\alpha^2 + dm\, k + d2dm\, m + g\, m + La\, d2alpha\, m\, \cos(\alpha) = -b\, ddm \quad (2)$$

2 Hand-editing within L^AT_EX

Making sense of the equations requires some hand editing. The equations are more easily understood when re-formatted *by hand* as shown below.

An improved latex expression for the first EOM is given below:

$$L_a m \left(L_a \ddot{\alpha} + (\ddot{d}_m + g) \cos(\alpha) \right) = \tau$$

This becomes:

$$L_a m \left(L_a \ddot{\alpha} + (\ddot{d}_m + g) \cos(\alpha) \right) = \tau \quad (3)$$

Similarly, the second equation can be written nicely as:

$$-L_a m \sin(\alpha) \dot{\alpha}^2 + d_m k + (\ddot{d}_m + g) m + L_a \ddot{\alpha} m \cos(\alpha) = -b \dot{d}_m$$

And this becomes:

$$-L_a m \sin(\alpha) \dot{\alpha}^2 + d_m k + (\ddot{d}_m + g) m + L_a \ddot{\alpha} m \cos(\alpha) = -b \dot{d}_m \quad (4)$$

Appendix: Example System

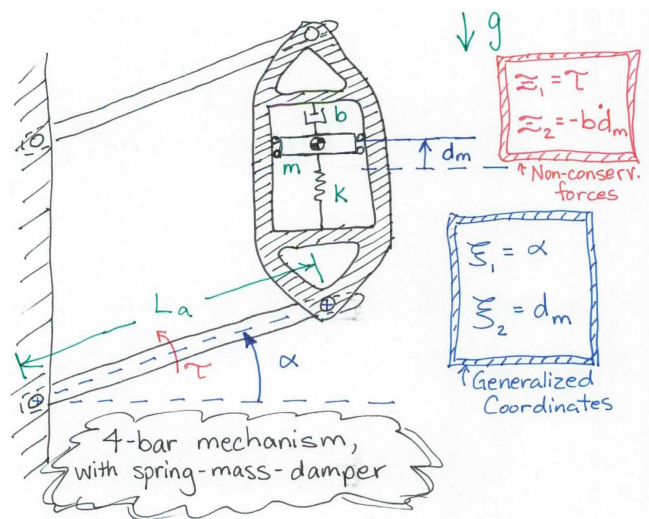


Figure 1: 4-bar mechanism with spring-mass-damper