

 6.3:
 $L_{eff}$ :

as For large  $L$ ,  $\tanh(\kappa L) \approx 1$ , which means that the result of the previous problem can be approximated

$$L_{eff} \approx \frac{1}{2\kappa}$$

 $L_p$ :

$$E(z) = A(z) e^{-j\beta_0 z} + B(z) e^{j\beta_0 z} \quad (6.25)$$

$$A(z) = A_1 e^{-\sigma z} + A_2 e^{\sigma z}$$

$$B(z) = B_1 e^{-\sigma z} + B_2 e^{\sigma z} \quad (6.28, 6.29)$$

For large  $L$ , the return power is approximately zero at the end of the grating. This gives us one boundary condition:

$$B(L) = 0 = B_1 e^{-\sigma L} + B_2 e^{\sigma L}$$

$$B_2 = -B_1 e^{-2\sigma L}$$

Then, by Eq. 6.30,

$$A_1 = \frac{j(\sigma + j\delta)}{\kappa} B_1$$

and

$$A_2 = \frac{j(\sigma - j\delta)}{\kappa} B_1 e^{-2\sigma L}$$

Condensing all of these equations, we can write

$$E(z) = \left( \frac{j(\sigma + j\delta)}{\kappa} B_1 e^{-\sigma z} + \frac{j(\sigma - j\delta)}{\kappa} B_1 e^{\sigma(z-2L)} \right) e^{-j\beta_0 z} + \left( B_1 e^{-\sigma z} + B_1 e^{\sigma(z-2L)} \right) e^{j\beta_0 z}$$

Simplify this expression using three substitutions:

$$e^{-2\sigma L} \approx 0 \quad \text{for large } L.$$

$$\delta = 0 \quad \text{at the Bragg wavelength.}$$

$$\sigma = \kappa \quad \text{at the Bragg wavelength.}$$

Then

$$E(z) = B_1 e^{-\kappa z} (j e^{-j\beta_0 z} + e^{j\beta_0 z})$$

Therefore, the field decay is proportional to  $e^{-\kappa z}$  and the power decay is proportional to  $e^{-2\kappa z}$ .

The definition of the penetration depth,  $L_p$ , is the length at which the field decays to  $\frac{1}{e}$  of its peak value:

$$e^{-2\kappa L_p} = e^{-1}$$

Thus, we see that, for large  $L$ ,

$$L_p = \frac{1}{2\kappa} \approx L_{eff}$$

6.4:

Plot  $\Gamma_{gth}$  vs.  $\delta$ 

$$\lambda = 1.55 \mu\text{m}$$

$$\langle \alpha_i \rangle = 15 \text{ cm}^{-1}$$

$$\kappa = 50 \text{ cm}^{-1}$$

Mode is aligned with DBR at  $1.55 \mu\text{m}$ .Consider  $\phi = 0, 90^\circ$ , and  $180^\circ$ and  $\kappa L_g = 0.5$  and  $1$ 

From chapter 2, we know that

$$\Gamma_{gth} = \langle \alpha_i \rangle + \frac{1}{L_a} \ln \left( \frac{1}{|r_1 r_{eff}|} \right) \quad (2.23)$$

The only unknown on the right side of this equation is  $r_{eff}$ :

$$r_{eff} = r_g + \frac{t_g^2 r_2}{1 - r_g r_2} \quad (6.46)$$

$$\tilde{r}_g = -j \frac{\tilde{\kappa}_{-1} \tanh(\tilde{\sigma} L_g)}{\tilde{\sigma} + j \tilde{\delta} \tanh(\tilde{\sigma} L_g)} \quad (6.37)$$

$$\tilde{t}_g = \frac{\tilde{\sigma} \text{sech}(\tilde{\sigma} L_g)}{\tilde{\sigma} + j \tilde{\delta} \tanh(\tilde{\sigma} L_g)} e^{-j \beta_0 L_g} \quad (6.40)$$

where

The phase term of  $t_g$  is accounted for in the expression for  $r_2$ . So  $e^{-j \beta_0 L_g} = 1$ .

$$r_1 = \sqrt{0.32}$$

$$r_2 = \sqrt{0.32} e^{j \phi_2}$$

$$\tilde{\sigma} = \sqrt{\kappa^2 - \tilde{\delta}^2}$$

(6.32)

$$\tilde{\delta} = \tilde{\beta} - \beta_0 = \frac{2\pi\bar{n}}{\lambda} - \frac{2\pi\bar{n}}{\lambda_0} + j \frac{\langle g \rangle_{xy} - \langle \alpha_i \rangle}{2}$$

(6.33)

$$\langle g \rangle_{xy} = 0 \text{ in DBR}$$

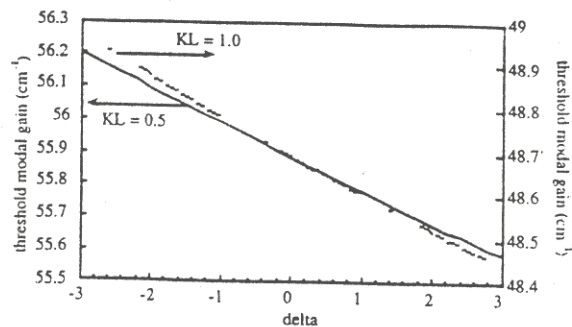
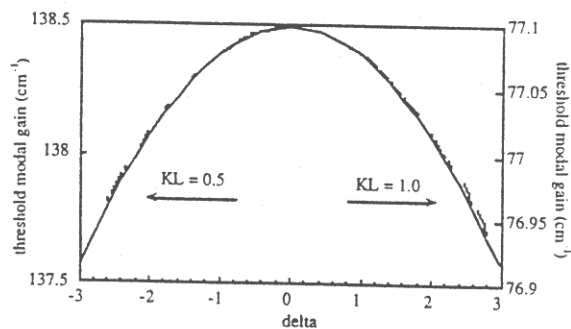
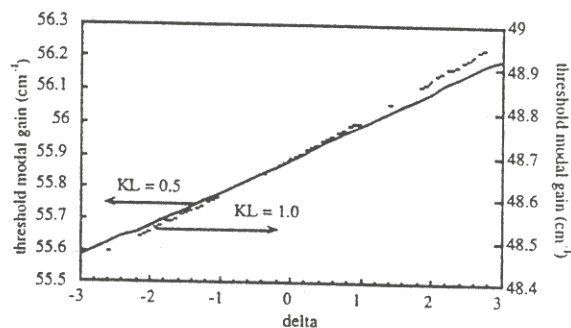
$$\langle \alpha_i \rangle = 15 \text{ cm}^{-1}$$

$$\rightarrow \tilde{\delta} = \delta - j \frac{\langle \alpha_i \rangle}{2}$$

$$\tilde{\kappa}_{-1} = \kappa = 50 \text{ cm}^{-1} \quad \text{since there is no perturbation of the loss or gain.}$$

$$L_g = \frac{\kappa L_a}{\kappa}$$

All of these equations can be combined to create an expression for threshold modal gain,  $\Gamma_{gth}$  in terms of the variables  $\kappa L_g$ ,  $\phi_2$ , and  $\delta$ .

Figure 6.4. Threshold modal gain vs. detuning for  $\phi_2 = 0^\circ$ .Figure 6.4. Threshold modal gain vs. detuning for  $\phi_2 = 90^\circ$ .Figure 6.4. Threshold modal gain vs. detuning for  $\phi_2 = 180^\circ$ .

$$\tilde{r}_g = -j \frac{\tilde{\kappa}_{-1} \tanh(\tilde{\sigma} L)}{\tilde{\sigma} + j \tilde{\delta} \tanh(\tilde{\sigma} L)} = |\tilde{r}_g| e^{j\phi} \quad (6.37)$$

The characteristic equation for a  $\frac{\lambda}{4}$  shifted DFB laser is

$$\tilde{r}_g^2 e^{-2j\tilde{\beta}L} = 1 \quad (\text{corrected 3.68})$$

where

$$L = \frac{\lambda}{2\tilde{n}} \quad (\text{see Fig. 3.17})$$

$$\tilde{\beta} = \frac{2\pi\tilde{n}}{\lambda} + j\frac{g-\alpha}{2}$$

Thus, the threshold condition is

$$\tilde{r}_g^2 e^{2\lambda(g-\alpha)/\tilde{n}} = 1$$

or

$$|\tilde{r}_g|^2 e^{2j\phi} e^{2\lambda(g-\alpha)/\tilde{n}} = 1$$

a) The characteristic equation is

$$\tilde{\sigma}_{th} = -j\tilde{\delta}_{th} \tanh(\tilde{\sigma}_{th} L_g) \quad (6.41)$$

$$\tilde{\sigma}_{th} = \sqrt{\kappa^2 - \tilde{\delta}_{th}^2}$$

$$\kappa = \frac{\kappa L}{L} = \frac{1}{400 \mu\text{m}} = 25 \text{ cm}^{-1}$$

$$\tilde{\delta}_{th} = \beta_{th} - \beta_0 + j \frac{\langle g \rangle_{xy} - \langle \alpha_i \rangle_{xy}}{2} = \Delta\beta + \frac{j\langle g \rangle_{xy}}{2}$$

$$\langle \alpha_i \rangle = 20 \text{ cm}^{-1}$$

Solve the characteristic equation given above for the two unknowns,  $\Delta\beta$  and  $\langle g \rangle_{xy}$ . Solve numerically:

First mode:

$$\Delta\beta = \pm 65 \text{ cm}^{-1}$$

$$\langle g \rangle_{xy} = 103 \text{ cm}^{-1}$$

$$\delta L = \Delta\beta L = \pm 2.6$$

Second mode:

$$\Delta\beta = \pm 141 \text{ cm}^{-1}$$

$$\langle g \rangle_{xy} = 152 \text{ cm}^{-1}$$

$$\delta L = \Delta\beta L = \pm 5.64$$

b) For a DFB with a  $\frac{\lambda}{4}$  shift, the characteristic equation is (neglecting gain across the short cavity length,  $\frac{\lambda}{2n}$ )

$$\tilde{r}_g^2 = 1$$

(Problem 6.6)

$$\tilde{r}_g = \frac{\kappa \tanh\left(\frac{\tilde{\sigma} L}{2}\right)}{\tilde{\sigma} + j\tilde{\delta} \tanh\left(\frac{\tilde{\sigma} L}{2}\right)} \quad (6.37)$$

Solving as in part (a), we get

First mode:

$$\Delta\beta = 0$$

$$\langle g \rangle_{xy} = 96 \text{ cm}^{-1}$$

$$\delta L = \Delta\beta L = 0$$

Second mode:

$$\Delta\beta = \pm 113 \text{ cm}^{-1}$$

$$\langle g \rangle_{xy} = 128 \text{ cm}^{-1}$$

$$\delta L = \Delta\beta L = \pm 4.52$$

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c) The mode supression ratio is given by

$$MSR = \left( \frac{\Delta\alpha + \Delta g}{\delta} + 1 \right) \frac{\alpha_m(\lambda_0)}{\alpha_m(\lambda_1)} \frac{F_1(\lambda_0)}{F_1(\lambda_1)} \quad (3.73, 3.74)$$

$$\frac{F_1(\lambda_0)}{F_1(\lambda_1)} \approx 1$$

$$\alpha_m = \langle g \rangle_{xy} - \langle \alpha_i \rangle$$

$$\Delta\alpha = \alpha_m(\lambda_1) - \alpha_m(\lambda_0)$$

$$\Delta g \approx 0 \text{ (since } \Delta\lambda \text{ is small, material gain is approximately constant over this wavelength range)}$$

$$\delta = \eta_r \beta_{sp} \langle g \rangle_{xy} \frac{I_{th}}{I - I_{th}} \quad (3.77)$$

We can use the threshold value of  $\langle g \rangle_{xy}$  because the gain is controlled by the carrier density, which is clamped at threshold.

Assume that

$$\eta_r = 1$$

$$\beta_{sp} = 10^{-4}$$

$$I = 2I_{th}$$

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case(a):

$$\delta = 10^{-4}(103 \text{ cm}^{-1}) = 0.0103 \text{ cm}^{-1}$$

$$\alpha_m(\lambda_0) = 103 - 20 = 83 \text{ cm}^{-1}$$

$$\alpha_m(\lambda_1) = 152 - 20 = 132 \text{ cm}^{-1}$$

$$\Delta\alpha = 132 - 83 = 49 \text{ cm}^{-1}$$

$$MSR = 2991$$

$$MSR(\text{ dB}) = 10 \log(MSR) = 34.8 \text{ dB}$$

---

case(b):

$$\delta = 10^{-4}(96 \text{ cm}^{-1}) = 0.0096 \text{ cm}^{-1}$$

$$\alpha_m(\lambda_0) = 96 - 20 = 76 \text{ cm}^{-1}$$

$$\alpha_m(\lambda_1) = 128 - 20 = 108 \text{ cm}^{-1}$$

$$\Delta\alpha = 108 - 76 = 32 \text{ cm}^{-1}$$

$$MSR = 2346$$

$$MSR(\text{ dB}) = 10 \log(MSR) = 33.7 \text{ dB}$$