

7.3:

$$\text{a) } V = k_0 d \sqrt{n_{\text{guide}}^2 - n_{\text{cladding}}^2} = \frac{2\pi}{1.55\mu\text{m}} (0.4\mu\text{m}) \sqrt{3.4^2 - 3.2^2} = 1.86 \quad (\text{A3.12})$$

$$a = 0$$

$$b = 0.40 \text{ from Fig. A3.2}$$

Solve Eq. A3.12 for $\bar{n}$

$$\bar{n} = \sqrt{n_c^2 + b(n_g^2 - n_c^2)} = \sqrt{3.2^2 + 0.40(3.4^2 - 3.2^2)} = 3.281$$

$$\begin{aligned} \theta_i &= \tan^{-1} \left(\frac{\beta}{k_{ix}} \right) \\ &= \tan^{-1} \left(\frac{k_0 \bar{n}}{k_0 \sqrt{n_g^2 - \bar{n}^2}} \right) \\ &= \tan^{-1} \left(\frac{3.281}{\sqrt{3.4^2 - 3.281^2}} \right) \\ &= 74.7^\circ \end{aligned}$$

b) For the same θ_i , $\bar{n}$, a , and b , we have, from Fig A3.2, for $m=1$,

$$V = 5.8$$

$$d = \frac{V}{k_0 \sqrt{n_g^2 - n_c^2}} = \frac{5.8}{\frac{2\pi}{1.55\mu\text{m}} \sqrt{3.4^2 - 3.2^2}} = 1.24\mu\text{m} \quad (\text{A3.12})$$

c)

$$a = \frac{n_{c2}^2 - n_{c1}^2}{n_g^2 - n_{c2}^2} = \frac{3.2^2 - 3^2}{3.4^2 - 3.2^2} = 0.939 \approx 1.0 \quad (\text{A3.12})$$

$$b = 0.40$$

From Fig. A3.2,

$$V = 2.2$$

$$d = \frac{V}{k_0 \sqrt{n_g^2 - n_c^2}} = \frac{2.2}{\frac{2\pi}{1.55\mu\text{m}} \sqrt{3.4^2 - 3.2^2}} = 0.47\mu\text{m} \quad (\text{A3.12})$$

7.4:

As described by Fig. 7.13, modes occur at resonances of the layer structure. The resonances can be found by using the transmission matrices of chapter 3 (see Table 3.3).

Assuming lossless material, the propagation matrices are given by

$$T_p = \begin{bmatrix} e^{j\beta_t L_t} & 0 \\ 0 & e^{-j\beta_t L_t} \end{bmatrix}$$

where

$$\beta_t = k_x = \sqrt{k_0^2 - k_z^2} = \frac{2\pi}{\lambda_0} \sqrt{n^2 - \bar{n}^2}$$

L_t = distance of propagation (i.e. thickness of layer).

The reflection matrices are given by

$$T_{r12} = \frac{1}{t_{12}} \begin{bmatrix} 1 & r_{12} \\ r_{12} & 1 \end{bmatrix}$$

$$r_{12} = \frac{n_1 - n_2}{n_1 + n_2}$$

$$t_{12} = \sqrt{1 - r_{12}^2}$$

The reflection values shown in Fig. 7.13,

$$r_A = r_B = \frac{T_{21}}{T_{11}}$$

$$T = T_{pa} T_{ra1} T_{p1} T_{r12} T_{p2} T_{r21} T_{p1} T_{r12}$$

Modes of the waveguide structure occur for

$$r_A^2 = 1$$

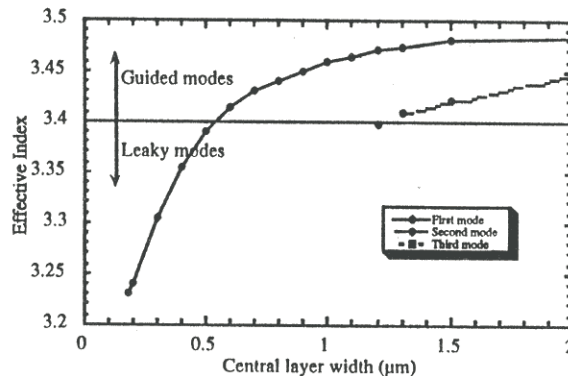


Figure 7.4. Effective index vs. central layer thickness



7.5:

For perfectly reflecting boundaries placed at $30\mu\text{m}$, $r = -1$. From Table 1.1, $n(\text{GaAs at } 1.0\mu\text{m}) = 3.52$ and $n(\text{Al}_{0.2}\text{Ga}_{0.8}\text{As at } 1.0\mu\text{m}) = 3.39$. This layer structure is shown in Fig. 7.11.

Solve for guided modes:

Guided modes can be solved for as done in Appendix 3. Using Eq. A3.12 and Fig. A3.2, we find that

$$V = \frac{2\pi}{1.0\mu\text{m}}(0.3\mu\text{m})\sqrt{3.52^2 - 3.39^2} = 1.79$$

So there is one guided mode.

$$b = 0.36$$

$$\bar{n} = \sqrt{3.39^2 + (0.36)(3.52^2 - 3.39^2)} = 3.437$$

$$\beta(m=1) = \frac{2\pi}{1.0\mu\text{m}}3.437 = 21.598$$

Solve for radiation modes:

$$k = \sqrt{k_x^2 + \beta^2}$$

$$k_x = \sqrt{k^2 - \beta^2} = \frac{2\pi}{\lambda}\sqrt{n^2 - \bar{n}^2}$$

In order to satisfy the characteristic equation (round trip gain = 1), we have

$$r_1 e^{k_{1x}d_1} e^{k_{2x}d_2} e^{k_{3x}d_3} r_2 e^{k_{1x}d_1} e^{k_{2x}d_2} e^{k_{3x}d_3} = 1$$

$$r_1 = r_2 = -1$$

$$d_1 = d_3 = 30\mu\text{m}$$

$$d_2 = 0.3\mu\text{m}$$

$$k_1 = k_3 = \frac{2\pi}{1.0\mu\text{m}}\sqrt{3.39^2 - \bar{n}^2}$$

$$k_2 = \frac{2\pi}{1.0\mu\text{m}}\sqrt{3.52^2 - \bar{n}^2}$$

The phase of the characteristic equation can be simplified to

$$m \frac{\lambda}{2} = (30\mu\text{m})\sqrt{3.39^2 - \bar{n}^2} + (0.3\mu\text{m})\sqrt{3.52^2 - \bar{n}^2} + (30\mu\text{m})\sqrt{3.39^2 - \bar{n}^2} \quad \text{for } m \geq 2$$

Solve for β using perturbation theory described in Chapter 6.

Simplify this expression by replacing the waveguide region with the same width of cladding material. This simplifies the expression for β significantly and allows us to write a closed form solution for β .

$$m \frac{\lambda}{2} \approx (60.3\mu\text{m}) \frac{\lambda}{2\pi} \sqrt{\left(\frac{2\pi n_1}{\lambda}\right)^2 - \beta^2}$$

$$\beta(m) \approx \sqrt{\left(\frac{2\pi n_1}{\lambda}\right)^2 - \left(\frac{m\pi}{60\mu\text{m}}\right)^2}$$

The perturbation due to the waveguide can then be added to the value of β for each mode:

$$\Delta\beta = \frac{\int \Delta\epsilon k_0^2 |U|^2 dA}{2\beta \int |U|^2 dA} \quad (6.9)$$

For odd numbered modes,

$$U(x) = A \cos(k_{x1m}x)$$

where A is a normalization coefficient and k_{x1m} is the value of the x component of the k vector for mode number m : $k_{x1m} = \sqrt{k_1^2 - \beta_m^2}$

Similarly, for even numbered modes,

$$U(x) = A \sin(k_{x1m}x)$$

The index perturbation is $\Delta\epsilon = 3.52^2 - 3.39^2 = 0.90$

$$k_0 = \frac{2\pi}{1.0\mu\text{m}} = 6.28\mu\text{m}^{-1}$$

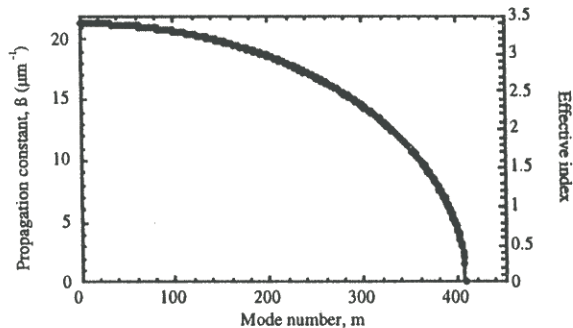


Figure 7.5. β and $\bar{n}$ vs. radiation mode number

Note: If better accuracy is desired, the values of β can be solved for numerically or graphically using the transcendental equations described by Eq. 7.26.



7.6:

Use Eq. 7.36 to implement the WKB method:

$$2 \int_{x=x_A}^{x=x_B} k_x(x) dx = (2m+1)\pi \quad (7.36)$$

Use symmetry to simplify this equation further

$$4 \int_0^{x=x_B} k_x(x) dx = (2m+1)\pi \quad (7.36)$$

$$k_x(x) = k_0 \sqrt{n^2(x) - \bar{n}^2}$$

$$n(x) = \begin{cases} \Delta n \left(1 - \frac{2x}{d}\right) + n_{\min} & 0 \leq x \leq \frac{d}{2} \\ \Delta n \left(1 + \frac{2x}{d}\right) + n_{\min} & -\frac{d}{2} \leq x \leq 0 \\ n_{\min} & \text{otherwise} \end{cases}$$

Rearrange this equation to solve for x_B (where $n(x) = \bar{n}$):

$$x_B = -x_A = \frac{d}{2} \left(1 - \frac{\bar{n} - n_{\min}}{n_{\max} - n_{\min}} \right)$$

Use computer to numerically plot right side of equation vs. $\bar{n}$. Values of $\bar{n}$ can then be chosen for each mode (i.e. $m = 1, 2, 3, \dots$).

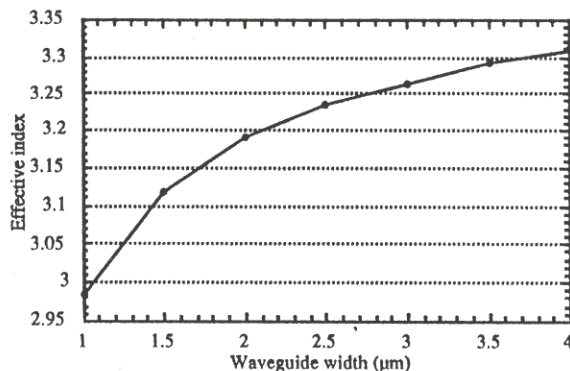


Figure 7.6. Effective index vs. waveguide width

The WKB approximation may not be accurate for $\bar{n}$ near $n_{\max}$ or $n_{\min}$.

Plot ray path:

$$\frac{\Delta x}{\Delta z} = \pm \tan \theta_i$$

$$\theta_i = \cos^{-1} \left(\frac{\bar{n}}{n(x)} \right)$$

$$d = 2\mu\text{m}$$

$$\bar{n} = 3.19 \quad \text{from part (a)}$$

At the center of the waveguide,

$$x = 0$$

$$\theta_i = \cos^{-1} \left(\frac{3.19}{3.5} \right) = 24.2^\circ$$

So in this case, we can't use the small angle approximation.

At the turnaround point,

$$x = x_B$$

$$n(x) = \bar{n}$$

$$\theta_i = \cos^{-1} \left(\frac{3.19}{3.19} \right) = 0^\circ$$

$$x_B = 0.124\mu\text{m}$$

To calculate the ray path, step along the path starting at

$$x_0 = 0$$

$$z_0 = 0$$

Using the recursive relation

$$x_{m+1} = x_m + \Delta z \tan \left[\cos^{-1} \left(\frac{\bar{n}}{n(x_m)} \right) \right]$$

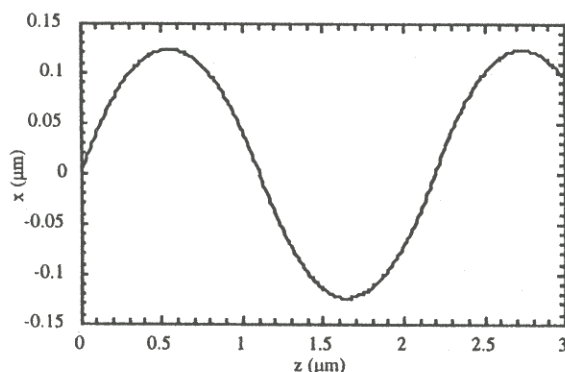


Figure 7.6. Ray path for the case of $d = 2$

Note that the curve is parabolic in shape (i.e. not a sine wave).