

Homework 4 (due 2/24)

4.1 Lagrangian equations of motion: Two-link pendulum.

- a) For the system shown in Figure 1, write expressions for T^* (the kinetic energy), for V (the potential energy) and for the Lagrangian: $\mathcal{L} = T^* - V$. (Hint: write expressions for the position of the mass [e.g., for x_m and y_m] and differentiate to find its velocity.)

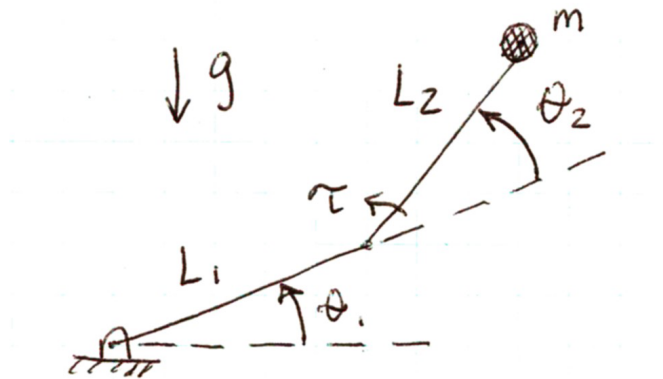


Figure 1: Double-link pendulum with point mass and torque (τ) at elbow.

- b) Find the equations of motion (EOMs) for the system. For each degree of freedom ($q_1 = \theta_1$, $q_2 = \theta_2$), $\Xi_i = \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{q}_i} - \frac{\partial \mathcal{L}}{\partial q_i}$. For this underactuated system, $\Xi_i = 0$ and the second actuation is $\Xi_i = \tau$. (τ appears in only the second EOM because we have used the *relative* angle at the elbow as the second degree of freedom.)

position and balance it about the vertical. The equations of motion for the Acrobot are

$$m_{11}\ddot{q}_1 + m_{12}\ddot{q}_2 + h_1 + \phi_1 = 0 \quad (51)$$

$$m_{21}\ddot{q}_1 + m_{22}\ddot{q}_2 + h_2 + \phi_2 = \tau_2 \quad (52)$$

where

$$m_{11} = m_1\ell_{c1}^2 + m_2(\ell_1^2 + \ell_{c2}^2 + 2\ell_1\ell_{c2}\cos(q_2)) + I_1 + I_2$$

$$m_{22} = m_2\ell_{c2}^2 + I_2$$

The simulations to follow were written in Simnon using the parameters in Table 1 below.

m_1	m_2	ℓ_1	ℓ_2	ℓ_{c1}	ℓ_{c2}	I_1	I_2	g
1	1	1	1	0.5	0.5	0.2	1.0	9.8

Table 1: Parameters of the Simulated Acrobot

Figure 2: Equations of motion for the acrobot, from [1] (p.381)

- c) This system is really just an acrobot. Show that your solution in part a) is identical to the equations of motion of an acrobot (described, for instance, in Spong's PFL paper [1]) if we use $m_1 = 0$, $L_2 = L_{c2}$, and $I_1 = I_2 = 0$. These equations of motion are shown in Figure 2.

4.2 Impedance of a wheel. Each of the wheels in Figure 3 has the same mass, $m = 1$ [kg], and radius, $R = 1$ [m], and each sits on the same downhill slope, γ [radians]. ($g = 9.81$ [m/s²]) However, each wheel has a different inertia. The wheel at left is a solid disk and has an inertia $J_a = \frac{1}{2}mR^2$. The center wheel is hollow, with all mass concentrated in a hoop at radius R , so $J_b = mR^2$. The wheel at right has all mass at a single point at its center, with massless spokes and rim, so $J_c = 0$.

- a) Write the equation of motion for each wheel using x (the position of the center of the wheel along the ramp direction) as the degree of freedom in each case.
b) What will the velocity, $\dot{x}$, of each wheel be 10 seconds after it is released from standstill?

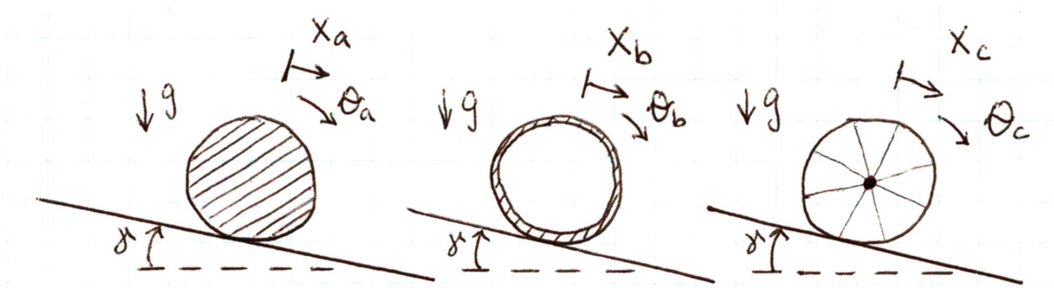


Figure 3: Three wheels, each with mass m and radius R .

4.3 Dynamics of spring-linked wheels. In this problem, we link the solid wheel ($J_a = \frac{1}{2}mR^2$) and the point-mass wheel ($J_c = 0$) from the previous problem with a spring of stiffness k . (Assume that with $x_1 = 0$ and $x_2 = 0$, the spring is at its undeflected length where it produces no force; otherwise, it is a linear spring: $F_k = k\Delta x$. Also assume the wheels roll with no slip.) Figure 4 shows the system.

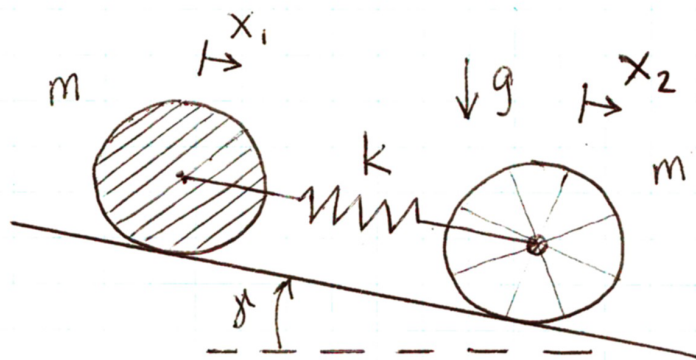


Figure 4: Solid wheel ($J = \frac{1}{2}mR^2$, at left) and point-mass wheel ($J = 0$) connected by a spring.

- a) Write the equations of motion of this system, using x_1 and x_2 as the two degrees of freedom.
- b) **Extra Credit** The total motion of the system can be thought of as the sum of 1) an acceleration downhill and 2) an oscillation. Namely, if the undeflected spring length when $x_1 = 0$ and $x_2 = 0$ is L , there is a location along the spring that travels with a constant acceleration, $x_{node} = x_1 + f(L + x_2)$. (If we were to paint a dot on the spring here, it would simply travel at a constant acceleration.) The motion of each mass is the sum of this constant acceleration plus an oscillation at some natural frequency, ω_n . (Each mass oscillates with the same frequency but at a different amplitude, of course.) Find expressions for:
- i) The fraction of the way from x_1 to x_2 , f , where the spring moves with constant acceleration.
- i) The natural frequency, ω_n .

4.4 Spring-mass-damper in series. Figure 5 shows a system with a mass ($F = m\ddot{x}$), a spring ($F = k\Delta x$), and a damper (aka “dashpot”, $F = b\Delta\dot{x}$) connected as shown. Using Laplace notation, the impedance (relating force to velocity at location i) of each can be written as:

$$Z_{mass} = ms, \text{ so } F_i = ms\dot{x}_i$$

$$Z_{damper} = b, \text{ so } F_i = b(\dot{x}_i - \dot{x}_j)$$

$$Z_{spring} = \frac{k}{s}, \text{ so } F_i = k(x_i - x_j)$$

(Note the force at x_i due to a damper/(spring) depends on a relative velocity/(position) with respect to another location (x_j) in the system.)

- b) Find the impedance relationship between F (the force) and $\dot{x}_3$ (the velocity where the force is applied):

$$Z_{tot} = \frac{F}{\dot{x}_3}.$$

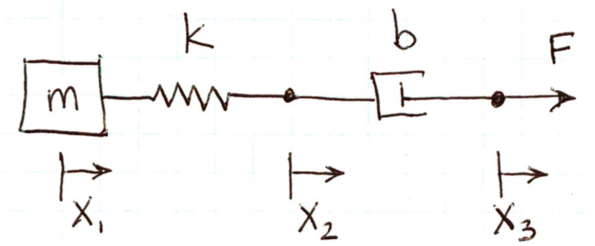


Figure 5: Spring-mass-damper system “in series”.

References

- [1] Mark W. Spong. Partial feedback linearization of underactuated mechanical systems. In *Proceedings of the IEEE International Conference on Intelligent Robots and Systems*, volume 1, pages 314–321, September 1994.