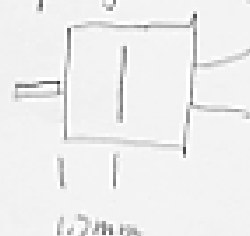


Base laser up against photodiode window



Feasible, but inconvenient. Move laser back 1 mm,
(as in packaged laser)



How much of 2D gaussian
does this circular PD
collect?

A. Can we assume PD is in the far field?

$$\theta = \frac{\lambda}{\pi w_0} \Rightarrow w_0 = \frac{\lambda}{\pi \theta}$$

Worst case half angles

$$\theta_{\parallel} = 13^\circ \quad \theta_{\perp} = 27^\circ$$

$$= 0.23 \text{ rad} \quad = 0.47 \text{ rad}$$

$$w_{0\parallel} = \frac{(405 \text{ nm})}{\pi (0.23 \text{ rad})} = 0.56 \mu$$

$$w_{0\perp} = \frac{(405)}{\pi (0.47)} = 0.27 \mu$$

The longest Rayleigh range

$$Z_r = \frac{\pi w_{0\perp}^2}{\lambda} = 2.4 \mu \quad \text{tiny compared to detector dist.}$$

$\therefore$ Far-field approximation is valid

(2)

Worst case estimate: assume the beam is circular, & diverges at the Θ_z angle:

$$w(z) = \frac{\lambda z}{\pi w_0} = \frac{(1.4 \mu)(2.7 \text{ Mm})}{\pi (0.27 \mu)} = 1.3 \text{ mm}$$

cf. pure geometrical case $w(z) = z \tan \Theta = 2.7 \text{ mm} \tan(27^\circ) = 1.37 \text{ mm}$

The fraction collected by the PD, radius $r = 1.5 \text{ mm}$

$$\frac{P(r)}{P(r=0)} = 1 - \exp\left[-\frac{2r^2}{w^2}\right] = 1 - \exp\left[-\frac{2(1.5 \text{ mm})^2}{(1.3 \text{ mm})^2}\right] = 0.93$$

$$\boxed{\text{Worst case collection efficiency} = 0.93}$$

cf. the result of numerical calculation over an elliptical beam & $\int_0^{2\pi} \int_0^r r' dr' \left[\exp\left(-\frac{2r'^2(w_z^2 \cos^2 \theta + w_y^2 \sin^2 \theta)}{w_z^2 w_y^2}\right) \right]$
(S. Srinivasan + others)

$$\rightarrow 0.96$$

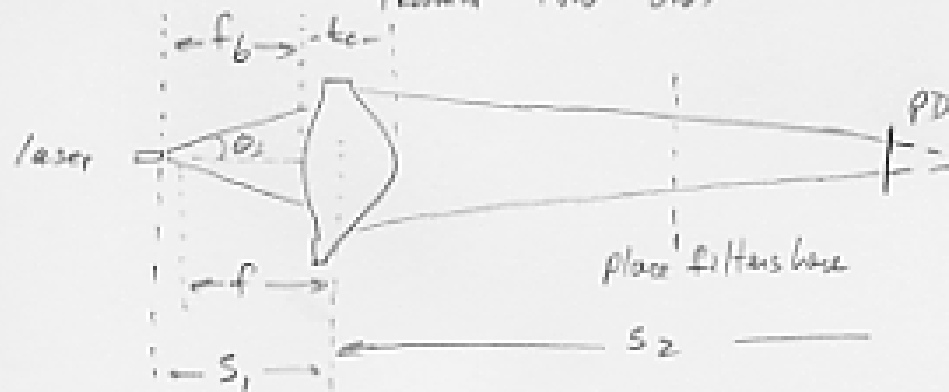
Thus, this photodetector can collect almost all the light. However, there is no room for filters, and probing can be difficult. Can we maintain the efficiency with a more convenient system?

2. Consider the Mellor Griot glass asphere,

(3)

AR coated 400-700 nm;

AK Coated 700-100 mm;						
LAG-18.0-12.0-C	f	ϕ	$f \Rightarrow NA$	f_b	t_c	
	12.0mm	18.0	0.67	0.75	6.9	8.8



For convenience, use $S_2 = 100$ mm

$$\frac{1}{S_1} + \frac{1}{S_2} = \frac{1}{f} \quad \text{In farfield, geometrical optics valid}$$

$$\frac{1}{S_1} = \frac{1}{f} - \frac{1}{S_2} = \frac{S_2 - f}{f S_2} \quad S_1 = \frac{f S_2}{S_2 - f} = \frac{(100 \text{ mm})(12 \text{ mm})}{(100 - 12) \text{ mm}} = 136 \text{ mm}$$

only slightly longer than f !

Note the lens surface is $f_b = 6.9$ mm from laser.

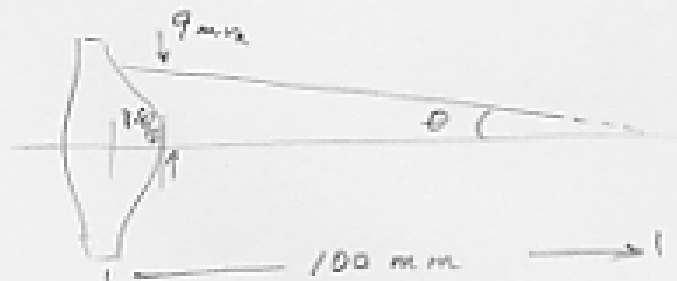
$$\begin{aligned} \text{Worst case (by geometrical optics): } W(\text{@lens}) &= (S_1 - \frac{t_c}{2}) \tan \theta_i \\ &= 9.2 \text{ mm} \tan(2^\circ) \\ &= 4.7 \text{ mm} \end{aligned}$$

$$\frac{P(\text{lens})}{P(\text{w})} = 1 - \exp\left(-\frac{2r^2}{w^2}\right) = 1 - \exp\left(-2\left(\frac{9.0}{4.7}\right)^2\right) = 0.999$$

$\therefore$ This collects all the light. What about at detector?

(4)

At the 3 mm ϕ detector, the maximum incident angle is



$$\theta_{\text{det}} \leq \tan^{-1}\left(\frac{9}{100-4.4}\right) = 5.4^\circ$$

$\therefore$ There is no worry about AR coating performance at large angles, or angular acceptance of package.

The asphere eliminates spherical aberration, which would be $\ll 3 \text{ mm } \phi$ anyway, and the diffraction limit $\sim \frac{\lambda}{NA} = \frac{.4 \mu}{\sin(5.4^\circ)} = 4 \mu$ is also of no concern.